

Stockholm University  
Department of Statistics  
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## **Econometrics I**

### **WRITTEN EXAMINATION**

Thursday April 27, 2017, 10 am - 3 pm

Allowed tools: Pocket calculator

Passing rate: 50% of overall total, which is 100 points. For detailed grading criteria, see the course description.

The exam will be handed back on Monday May 15 at 3 pm in room B705.

For the maximum number of points on each problem detailed and clear solutions are required.

If not indicated otherwise, the disturbance terms  $u_i$  in the models are supposed to fulfill the usual requirements of normality, homoscedasticity and independence.

You may answer in Swedish.

1. (25p) One wants to study the effective life time  $Y$  (in minutes) of a cutting tool on a lathe, with speed  $X$  (in rounds per minute), where we have access to two types of tools (A and B).

We assume the following model:

$$Y_i = \beta_1 + \beta_2 X_i + \beta_3 D_i + u_i.$$

where

$$D_i = \begin{cases} 1 & \text{if type B} \\ 0 & \text{if type A} \end{cases}$$

For data where we have used 10 tools of type A and 10 tools of type B ( $n = 20$ ), we got the following results:

| ANOVA            |                |    |
|------------------|----------------|----|
| Source           | Sum of Squares | df |
| Regression (SSE) | 1418.034       | 2  |
| Residuals (SSR)  | 157.055        | 17 |
| Total (SST)      | 1575.089       | 19 |

| Coefficients Table |             |                 |
|--------------------|-------------|-----------------|
| Variable           | Coefficient | SE( $\beta_i$ ) |
| Constant           | 36.986      |                 |
| $X$                | -0.027      | 0.005           |
| $D$                | 15.004      | 1.36            |

- Compute both coefficients of (multiple) determination (nonadjusted and adjusted).
- Investigate by a test if at least one of the explanatory variables should be included in the model. Use proper notation and state clearly the null and alternative hypotheses. Use significance level 1%.
- How do you interpret the parameter  $\beta_3$  in terms of expectation?
- Compute a 95% confidence interval for  $\beta_3$ .
- An alternative model is

$$Y_i = \beta'_1 + \beta'_2 X_i + \beta'_3 D_i + \beta'_4 X_i D_i + u'_i.$$

Describe the difference between the two models, that is, in what specific way is the second model more flexible ("richer")?

- The alternative second model was also used for estimation with the same data. Results:

| ANOVA            |                |    |
|------------------|----------------|----|
| Source           | Sum of Squares | df |
| Regression (SSE) | 1434.112       | 3  |
| Residuals (SSR)  | 140.977        | 16 |
| Total (SST)      | 1575.089       | 19 |

| Coefficients Table |             |                 |
|--------------------|-------------|-----------------|
| Variable           | Coefficient | SE( $\beta_i$ ) |
| Constant           | 32.775      |                 |
| $X$                | -0.021      | 0.0061          |
| $D$                | 23.971      | 6.769           |
| $XD$               | -0.012      | 0.088           |

Is the second model significantly better than the first model? Use significance level 5% with a suitable test.

2. (25p) The Cobb-Douglas production function is

$$Q = \beta_1 L^{\beta_2} K^{\beta_3}, \quad (1)$$

where  $L$  = labour input and  $K$  = capital stock.

Now, we want to use  $Y = \ln(Q)$  as dependent variable in a linear regression model.

- Write down a linear regression model based on (2) using  $Y$  as defined above.
- Now let  $\beta_3 = 1 - \beta_2$ . Rewrite the linear model according to this.
- Without doing any computation (since we do not have the numerical results, except that we assume that  $n = 33$ ), describe which test you would use for comparing the model in (a) with the model in (b).

In doing so, describe the null hypothesis, the test statistic with its parameters and for which values of the test statistic you should reject the null hypothesis.

- Mention one potential advantage, from a regression modelling point of view, of using the model in (b) instead of the model in (a).
- Using data from the years 1899 to 1922, we got that using the model in (a), the residual-based estimated autocorrelation coefficient  $\hat{\rho} = 0.6$ . Can we from this draw the conclusion that we have evidence of positive autocorrelation at (approximate) significance level 1%?

3. (20p) In order to investigate what proportion (on average) of the income a person spends on the rent of a flat in New York, data were collected from 108 single households. A simple linear regression model was estimated using rent as dependent variable ( $Y$ ) and income as independent variable ( $X$ ). One suspects problems with heteroscedasticity. White's test was performed with the following results:

### White's Auxiliary Regression

Included Observations: 108

| Variable            | Coefficient | Std. Error            | t-Statistic | Prob.    |
|---------------------|-------------|-----------------------|-------------|----------|
| C                   | -14657900   | 9288994               | -1.577986   | 0.1176   |
| INCOME              | 1200.579    | 495.1663              | 2.424598    | 0.0170   |
| INCOME <sup>2</sup> | -0.010007   | 0.005355              | -1.868714   | 0.0644   |
| R-squared           | 0.082134    | Mean dependent var    |             | 10515952 |
| Adjusted R-squared  | 0.064651    | S.D. dependent var    |             | 29847739 |
| S.E. of regression  | 28866783    | Akaike info criterion |             | 37.22167 |
| Sum squared resid   | 8.75E + 16  | Schwarz criterion     |             | 37.29617 |
| Log likelihood      | -2006.970   | F-statistic           |             | 4.697874 |
| Durbin-Watson stat  | 1.864571    | Prob(F-statistic)     |             | 0.011115 |

- Write down the auxiliary regression model used in this situation for White's test with proper notation.
- Show that we can reject the null hypothesis of homoscedasticity at significance level 5%.
- It turns out that we can model the variance of the disturbance variable as  $V(u_i) = \sigma^2 X_i$ . How can we take this into account to obtain a homoscedastic model?

4. (12p) The "true" model given specific data is supposed to be

$$Y_i = \beta_1 + \beta_2 X_i + u_i$$

For some reason though, the following model is used for estimation of the  $\beta$ -parameters:

$$(Y_i - c_1) = \beta_1 + \beta_2(X_i - c_2) + u_i,$$

where  $c_1$  and  $c_2$  are given (known) constants.

- (a) Derive expressions for the OLS-estimators of  $\beta_1$  and  $\beta_2$  using the second "wrong" model.
  - (b) Are both estimators from (a) unbiased?
5. (18p) True or false statements? Short motivation/comment also needed.
- (a) If  $X_i$  in the model  $Y_i = \beta_1 + \beta_2 X_i + u_i$  is divided by 2, both estimators  $\hat{\beta}_1$  and  $\hat{\beta}_2$  are changed.
  - (b) If we in the model  $Y_i = \beta_1 + \beta_2 X_i + u_i$  have a measurement error in  $Y_i$ , then  $Cov(X_i, u_i) \neq 0$ .
  - (c) The Durbin-Watson test cannot be used if the disturbance variables are autocorrelated.
  - (d) For two random variables,  $X_i$  and  $Y_i$ , we always have that  $-1 \leq Cov(X_i, Y_i) \leq 1$ .
  - (e) Heteroscedasticity occurs when the disturbance term in a regression model is correlated with one of the explanatory variables.
  - (f) In the Runs test, the number of runs is asymptotically normally distributed.

Svensk version:

10. (25p) Man önskar studera den effektiva livslängden  $Y$  (i minuter) för ett skärverktyg på en svarv med hastighet  $X$  (varv per minut), där vi har tillgång till två typer av verktyg (A och B).

Vi antar följande modell:

$$Y_i = \beta_1 + \beta_2 X_i + \beta_3 D_i + u_i.$$

där

$$D_i = \begin{cases} 1 & \text{om typ B} \\ 0 & \text{om typ A} \end{cases}$$

För data där vi använt 10 verktyg av typ A och 10 verktyg av typ B ( $n = 20$ ), erhöles följande resultat:

| ANOVA            |                |    |
|------------------|----------------|----|
| Source           | Sum of Squares | df |
| Regression (SSE) | 1418.034       | 2  |
| Residuals (SSR)  | 157.055        | 17 |
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| Coefficients Table |             |                       |
|--------------------|-------------|-----------------------|
| Variable           | Coefficient | SE( $\hat{\beta}_i$ ) |
| Constant           | 36.986      |                       |
| $X$                | -0.027      | 0.005                 |
| $D$                | 15.004      | 1.36                  |

- Beräkna både den ojusterade och justerade (multipla) förklaringsgraden.
- Undersök med ett test om minst en av förklaringsvariablerna ska ingå i modellen. Använd lämplig notation och klargör tydligt noll- och mothypotes. Använd signifikansnivå 1%.
- Hur tolkar du parametern  $\beta_3$  i i väntevärdesmening?
- Beräkna ett 95% konfidensintervall för  $\beta_3$ .
- En alternativ modell är

$$Y_i = \beta_1' + \beta_2' X_i + \beta_3' D_i + \beta_4' X_i D_i + u_i'.$$

Beskriv skillnaden mellan de två modellerna, dvs, i vilken specifik mening är den andra modellen mer flexibel ("rikare")?

- Också den alternativa modellen användes för skattning med samma data. Resultat:

| ANOVA            |                |    |
|------------------|----------------|----|
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| Regression (SSE) | 1434.112       | 3  |
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Är den andra modellen signifikant bättre än den första modellen?  
Använd signifikansnivå 5% med lämpligt test.

24. (25p) Cobb-Douglas produktionsfunktion är

$$Q = \beta_1 L^{\beta_2} K^{\beta_3}, \quad (2)$$

där  $L$  = "labour input" and  $K$  = "capital stock".

Vi vill nu använda  $Y = \ln(Q)$  som beroende variabel i en linjär regressionsmodell.

- Skriv ner en linjär regressionsmodell baserad på (2) och  $Y$  definierad enligt ovanstående.
- Låt nu  $\beta_3 = 1 - \beta_2$ . Skriv om den linjära modellen enligt denna restriktion.
- Utan att utföra någon beräkning (eftersom vi inte har några numeriska resultat, förutom att vi antar att  $n = 33$ ), beskriv vilket test du skulle använda vid jämförelse av modellen i (a) med modellen i (b). Beskriv i samband med detta nollhypotesen, teststatistikan med dess parametrar och för vilka värden på teststatistikan som nollhypotesen förkastas.
- Nämna en potentiell fördel, från ett regressionsmodellperspektiv, med att använda modellen i (b) i stället för modellen i (a).
- Genom att använda årsdata för åren 1899 till 1922, fick vi genom att använda modellen i (a) att den residual-baserade skattade autokorrelationskoefficienten  $\hat{\rho} = 0.6$ . Kan vi från detta dra slutsatsen att vi kan påvisa positiv autokorrelation på (approximativ) signifikansnivå 1%?

38. (20p) För att undersöka den genomsnittliga andelen av inkomsten som en person spenderar på hyran för en lägenhet i New York, samlades data in från 108 singelhushåll. En enkel linjär regressionsmodell skattades med hyran som beroende variabel ( $Y$ ) och inkomst som oberoende variabel ( $X$ ). Man misstänker problem med heteroskedasticitet. Whites test användes med följande resultat:

White's Auxiliary Regression

Included Observations: 108

| Variable            | Coefficient | Std. Error            | t-Statistic | Prob.    |
|---------------------|-------------|-----------------------|-------------|----------|
| C                   | -14657900   | 9288994               | -1.577986   | 0.1176   |
| INCOME              | 1200.579    | 495.1663              | 2.424598    | 0.0170   |
| INCOME <sup>2</sup> | -0.010007   | 0.005355              | -1.868714   | 0.0644   |
| R-squared           | 0.082134    | Mean dependent var    |             | 10515952 |
| Adjusted R-squared  | 0.064651    | S.D. dependent var    |             | 29847739 |
| S.E. of regression  | 28866783    | Akaike info criterion |             | 37.22167 |
| Sum squared resid   | 8.75E+16    | Schwarz criterion     |             | 37.29617 |
| Log likelihood      | -2006.970   | F-statistic           |             | 4.697874 |
| Durbin-Watson stat  | 1.864571    | Prob(F-statistic)     |             | 0.011115 |

- Skriv ner den auxiliära regressionsmodellen som använts i den här situationen för Whites test med lämplig notation.
- Visa att vi kan förkasta nollhypotesen om homoskedasticitet på signifikansnivå 5%.
- Det visar sig att vi kan modellera variansen för störningsvariabeln som  $V(u_i) = \sigma^2 X_i$ . Hur kan vi utnyttja detta för att åstadkomma en homoskedastisk modell?



4. (12p) Den "sanna" modellen givet specifik data antas vara

$$Y_i = \beta_1 + \beta_2 X_i + u_i$$

Av någon anledning används dock följande modell för skattning av  $\beta$ -parametrarna.

$$(Y_i - c_1) = \beta_1 + \beta_2(X_i - c_2) + u_i,$$

där  $c_1$  och  $c_2$  är givna (kända) konstanter.

- Härled uttryck för OLS-skattningarna av  $\beta_1$  och  $\beta_2$  när "fel" modell används.
- Är bägge skattningarna i (a) väntevärdesriktiga?

5. (20p) Sanna eller falska påståenden? Korta motiveringar/kommentarer behövs.

- Om  $X_i$  i modellen  $Y_i = \beta_1 + \beta_2 X_i + u_i$  divideras med 2, ändras både  $\hat{\beta}_1$  and  $\hat{\beta}_2$ .
- Om vi i modellen  $Y_i = \beta_1 + \beta_2 X_i + u_i$  har mätfel i  $Y_i$ , så är  $Cov(X_i, u_i) \neq 0$ .
- Durbin-Watson testet kan inte användas om vi har autokorrelerade störningsvariabler.
- För två stokastiska variabler  $X_i$  och  $Y_i$ , gäller alltid att  $-1 \leq Cov(X_i, Y_i) \leq 1$ .
- Heteroskedasticitet inträffar när störningsvariabeln i en regressionsmodell är korrelerad med en av de förklarande variablerna.
- I Runstestet är antalet "runs" asymptotiskt normalfördelat.

## Formula sheet, Econometrics I, Spring 2017

Under the simple linear model  $Y_i = \beta_1 + \beta_2 X_i + u_i$ , where  $u_i \sim N(0, \sigma^2)$  and given independent pairs of observations  $(Y_1, X_1), \dots, (Y_n, X_n)$ , the OLS (and ML) estimators are:

$$\begin{aligned}\hat{\beta}_1 &= \bar{Y} - \hat{\beta}_2 \bar{X} \\ \hat{\beta}_2 &= \frac{\sum (X_i - \bar{X})(Y_i - \bar{Y})}{\sum (X_i - \bar{X})^2} \\ \hat{\sigma}^2 &= \frac{RSS}{n-2} = \frac{\sum (Y_i - \hat{Y}_i)^2}{n-2}\end{aligned}$$

where  $\hat{Y}_i = \hat{\beta}_1 + \hat{\beta}_2 X_i$  and where  $E(\hat{\beta}_1) = \beta_1$ ,  $E(\hat{\beta}_2) = \beta_2$  and  $E(\hat{\sigma}^2) = \sigma^2$  and further

$$\begin{aligned}V(\hat{\beta}_1) &= \frac{\sum X_i^2}{n \sum (X_i - \bar{X})^2} \sigma^2 \\ V(\hat{\beta}_2) &= \frac{\sigma^2}{\sum (X_i - \bar{X})^2} \\ V(\hat{Y}_0) &= \sigma^2 \left( \frac{1}{n} + \frac{(X_0 - \bar{X})^2}{\sum (X_i - \bar{X})^2} \right) \\ V(Y_0 - \hat{Y}_0) &= \sigma^2 \left( 1 + \frac{1}{n} + \frac{(X_0 - \bar{X})^2}{\sum (X_i - \bar{X})^2} \right)\end{aligned}$$

Distributional results:

$$\begin{aligned}\frac{\hat{\beta}_i - \beta_i}{se(\hat{\beta}_i)} &\sim t(n-2), \quad i = 1, 2 \\ \frac{\hat{\sigma}^2 (n-2)}{\sigma^2} &\sim \chi^2(n-2)\end{aligned}$$

Coefficient of determination:

$$r^2 = \frac{ESS}{TSS} = 1 - \frac{RSS}{TSS} = 1 - \frac{\sum (Y_i - \hat{Y}_i)^2}{\sum (Y_i - \bar{Y})^2}$$

Coefficient of correlation:

$$r = \frac{\sum (X_i - \bar{X})(Y_i - \bar{Y})}{\sqrt{\sum (X_i - \bar{X})^2 \sum (Y_i - \bar{Y})^2}}$$

where  $r = \pm\sqrt{r^2}$

If we let  $Y_i^* = w_1 Y_i$  and  $X_i^* = w_2 X_i$ , then

$$\hat{\beta}_1^* = w_1 \hat{\beta}_1, \quad \hat{\beta}_2^* = \left(\frac{w_1}{w_2}\right) \hat{\beta}_2, \quad \hat{\sigma}^{*2} = w_1^2 \hat{\sigma}^2$$

Under the multiple linear regression model  $Y_i = \beta_1 + \beta_2 X_{2i} + \dots + \beta_k X_{ki} + u_i$ , where  $u_i \sim N(0, \sigma^2)$  and given independent vectors of observations  $(Y_1, X_{21}, \dots, X_{k1}), \dots, (Y_n, X_{2n}, \dots, X_{kn})$ , the following holds for the OLS (ML) estimators:

$$\hat{\sigma}^2 = \frac{RSS}{n-k} = \frac{\sum (Y_i - \hat{Y}_i)^2}{n-k}$$

$$\frac{\hat{\beta}_i - \beta_i}{se(\hat{\beta}_i)} \sim t(n-k), \quad i = 1, \dots, k$$

$$\frac{\hat{\sigma}^2 (n-k)}{\sigma^2} \sim \chi^2(n-k)$$

The multiple coefficient of determination:

$$R^2 = \frac{ESS}{TSS} = 1 - \frac{RSS}{TSS} = 1 - \frac{\sum (Y_i - \hat{Y}_i)^2}{\sum (Y_i - \bar{Y})^2}$$

Adjusted:

$$\bar{R}^2 = 1 - \frac{RSS/(n-k)}{TSS/(n-1)}$$

Testing  $H_0: \beta_2 = \dots = \beta_k = 0$ :

$$F = \frac{ESS/(k-1)}{RSS/(n-k)} = \frac{\sum (\hat{Y}_i - \bar{Y})^2 / (k-1)}{\sum (Y_i - \hat{Y}_i)^2 / (n-k)}$$

Comparing an "old" model with a "new" (larger):

$$F = \frac{(ESS_{new} - ESS_{old})/\text{number of new regressors}}{RSS_{new}/(n - \text{number of parameters in the new model})}$$

$$= \frac{(R_{new}^2 - R_{old}^2)/\text{number of new regressors}}{(1 - R_{new}^2)/(n - \text{number of parameters in the new model})}$$

Comparing an "unrestricted" model with a "restricted":

$$F = \frac{(RSS_R - RSS_{UR})/m}{RSS_{UR}/(n-k)} = \frac{(R_{UR}^2 - R_R^2)/m}{(1 - R_{UR}^2)/(n-k)}$$

where  $m$  is the number of linear constraints and  $k$  is the number of parameters in the unrestricted model.

Variance inflation factor:

$$VIF_j = \frac{1}{1 - R_j^2}$$

Auxiliary regression:

$$F_j = \frac{R_j^2/(k-2)}{(1 - R_j^2)/(n-k+1)}$$

where  $R_j^2 = R^2$  in the regression of the remaining  $(k-2)$  regressors.

White's test for heteroscedasticity:

$$n R^2 \stackrel{\text{appr}}{\sim} \chi^2 (df = \text{number of regressors in the auxiliary regression})$$

(Holds under  $H_0$ : no heteroscedasticity.)

For  $R$  = number of runs, where  $N = N_1 + N_2$  total number of observations:

$$E(R) = \frac{2N_1N_2}{N} + 1$$
$$V(R) = \frac{2N_1N_2(2N_1N_2 - N)}{N^2(N-1)}$$

The Durbin Watson  $d$  statistic:

$$d = \frac{\sum_{t=2}^n (\hat{u}_t - \hat{u}_{t-1})^2}{\sum_{t=1}^n \hat{u}_t^2}$$

Akaike's information criterion:

$$AIC = \frac{e^{2k/n} RSS}{n}$$

Schwartz's information criterion:

$$SIC = \frac{n^{k/n} RSS}{n}$$

Mallow's  $C_p$  criterion:

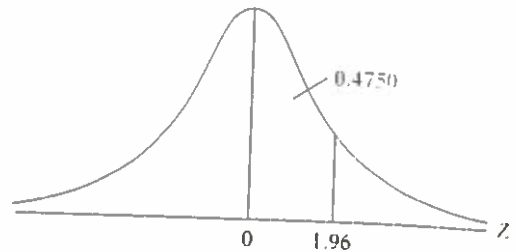
$$C_p = \frac{RSS_p}{\hat{\sigma}^2} - (n - 2p)$$

**TABLE D.1**  
Areas Under the  
Standardized Normal  
Distribution

**Example**

$$\Pr(0 \leq Z \leq 1.96) = 0.4750$$

$$\Pr(Z \geq 1.96) = 0.5 - 0.4750 = 0.025$$



| Z   | .00   | .01   | .02   | .03   | .04   | .05   | .06   | .07   | .08   | .09   |
|-----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.0 | .0000 | .0040 | .0080 | .0120 | .0160 | .0199 | .0239 | .0279 | .0319 | .0359 |
| 0.1 | .0398 | .0438 | .0478 | .0517 | .0557 | .0596 | .0636 | .0675 | .0714 | .0753 |
| 0.2 | .0793 | .0832 | .0871 | .0910 | .0948 | .0987 | .1026 | .1064 | .1103 | .1141 |
| 0.3 | .1179 | .1217 | .1255 | .1293 | .1331 | .1368 | .1406 | .1443 | .1480 | .1517 |
| 0.4 | .1554 | .1591 | .1628 | .1664 | .1700 | .1736 | .1772 | .1808 | .1844 | .1879 |
| 0.5 | .1915 | .1950 | .1985 | .2019 | .2054 | .2088 | .2123 | .2157 | .2190 | .2224 |
| 0.6 | .2257 | .2291 | .2324 | .2357 | .2389 | .2422 | .2454 | .2486 | .2517 | .2549 |
| 0.7 | .2580 | .2611 | .2642 | .2673 | .2704 | .2734 | .2764 | .2794 | .2823 | .2852 |
| 0.8 | .2881 | .2910 | .2939 | .2967 | .2995 | .3023 | .3051 | .3078 | .3106 | .3133 |
| 0.9 | .3159 | .3186 | .3212 | .3238 | .3264 | .3289 | .3315 | .3340 | .3365 | .3389 |
| 1.0 | .3413 | .3438 | .3461 | .3485 | .3508 | .3531 | .3554 | .3577 | .3599 | .3621 |
| 1.1 | .3643 | .3665 | .3686 | .3708 | .3729 | .3749 | .3770 | .3790 | .3810 | .3830 |
| 1.2 | .3849 | .3869 | .3888 | .3907 | .3925 | .3944 | .3962 | .3980 | .3997 | .4015 |
| 1.3 | .4032 | .4049 | .4066 | .4082 | .4099 | .4115 | .4131 | .4147 | .4162 | .4177 |
| 1.4 | .4192 | .4207 | .4222 | .4236 | .4251 | .4265 | .4279 | .4292 | .4306 | .4319 |
| 1.5 | .4332 | .4345 | .4357 | .4370 | .4382 | .4394 | .4406 | .4418 | .4429 | .4441 |
| 1.6 | .4452 | .4463 | .4474 | .4484 | .4495 | .4505 | .4515 | .4525 | .4535 | .4545 |
| 1.7 | .4454 | .4564 | .4573 | .4582 | .4591 | .4599 | .4608 | .4616 | .4625 | .4633 |
| 1.8 | .4641 | .4649 | .4656 | .4664 | .4671 | .4678 | .4686 | .4693 | .4699 | .4706 |
| 1.9 | .4713 | .4719 | .4726 | .4732 | .4738 | .4744 | .4750 | .4756 | .4761 | .4767 |
| 2.0 | .4772 | .4778 | .4783 | .4788 | .4793 | .4798 | .4803 | .4808 | .4812 | .4817 |
| 2.1 | .4821 | .4826 | .4830 | .4834 | .4838 | .4842 | .4846 | .4850 | .4854 | .4857 |
| 2.2 | .4861 | .4864 | .4868 | .4871 | .4875 | .4878 | .4881 | .4884 | .4887 | .4890 |
| 2.3 | .4893 | .4896 | .4898 | .4901 | .4904 | .4906 | .4909 | .4911 | .4913 | .4916 |
| 2.4 | .4918 | .4920 | .4922 | .4925 | .4927 | .4929 | .4931 | .4932 | .4934 | .4936 |
| 2.5 | .4938 | .4940 | .4941 | .4943 | .4945 | .4946 | .4948 | .4949 | .4951 | .4952 |
| 2.6 | .4953 | .4955 | .4956 | .4957 | .4959 | .4960 | .4961 | .4962 | .4963 | .4964 |
| 2.7 | .4965 | .4966 | .4967 | .4968 | .4969 | .4970 | .4971 | .4972 | .4973 | .4974 |
| 2.8 | .4974 | .4975 | .4976 | .4977 | .4977 | .4978 | .4979 | .4979 | .4980 | .4981 |
| 2.9 | .4981 | .4982 | .4982 | .4983 | .4984 | .4984 | .4985 | .4985 | .4986 | .4986 |
| 3.0 | .4987 | .4987 | .4987 | .4988 | .4988 | .4989 | .4989 | .4989 | .4990 | .4990 |

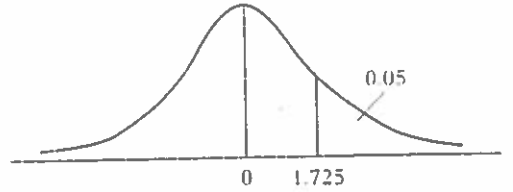
*Note:* This table gives the area in the right-hand tail of the distribution (i.e.,  $Z \geq 0$ ). But since the normal distribution is symmetrical about  $Z = 0$ , the area in the left-hand tail is the same as the area in the corresponding right-hand tail. For example,  $\Pr(-1.96 \leq Z \leq 0) = 0.4750$ . Therefore,  $\Pr(-1.96 \leq Z \leq 1.96) = 2(0.4750) = 0.95$ .

**TABLE 12**  
**Percentage Points of**  
**the *t* Distribution**

Source: From F. S. Pearson and H. O. Hartley, eds., *Biometrika Tables for Statisticians*, vol. 1, 3d ed., table 12, Cambridge University Press, New York, 1966. Reproduced by permission of the editors and trustees of *Biometrika*.

**Example**

$\Pr(t > 2.086) = 0.025$   
 $\Pr(t > 1.725) = 0.05$  for  $df = 20$   
 $\Pr(|t| > 1.725) = 0.10$



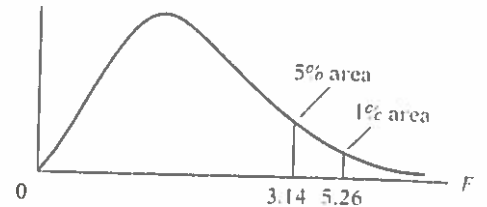
| Pr<br>df | 0.25<br>0.50 | 0.10<br>0.20 | 0.05<br>0.10 | 0.025<br>0.05 | 0.01<br>0.02 | 0.005<br>0.010 | 0.001<br>0.002 |
|----------|--------------|--------------|--------------|---------------|--------------|----------------|----------------|
| 1        | 1.000        | 3.078        | 6.314        | 12.706        | 31.821       | 63.657         | 318.31         |
| 2        | 0.816        | 1.886        | 2.920        | 4.303         | 6.965        | 9.925          | 22.327         |
| 3        | 0.765        | 1.638        | 2.353        | 3.182         | 4.541        | 5.841          | 10.214         |
| 4        | 0.741        | 1.533        | 2.132        | 2.776         | 3.747        | 4.604          | 7.173          |
| 5        | 0.727        | 1.476        | 2.015        | 2.571         | 3.365        | 4.032          | 5.893          |
| 6        | 0.718        | 1.440        | 1.943        | 2.447         | 3.143        | 3.707          | 5.208          |
| 7        | 0.711        | 1.415        | 1.895        | 2.365         | 2.998        | 3.499          | 4.785          |
| 8        | 0.706        | 1.397        | 1.860        | 2.306         | 2.896        | 3.355          | 4.501          |
| 9        | 0.703        | 1.383        | 1.833        | 2.262         | 2.821        | 3.250          | 4.297          |
| 10       | 0.700        | 1.372        | 1.812        | 2.228         | 2.764        | 3.169          | 4.144          |
| 11       | 0.697        | 1.363        | 1.796        | 2.201         | 2.718        | 3.106          | 4.025          |
| 12       | 0.695        | 1.356        | 1.782        | 2.179         | 2.681        | 3.055          | 3.930          |
| 13       | 0.694        | 1.350        | 1.771        | 2.160         | 2.650        | 3.012          | 3.852          |
| 14       | 0.692        | 1.345        | 1.761        | 2.145         | 2.624        | 2.977          | 3.787          |
| 15       | 0.691        | 1.341        | 1.753        | 2.131         | 2.602        | 2.947          | 3.733          |
| 16       | 0.690        | 1.337        | 1.746        | 2.120         | 2.583        | 2.921          | 3.686          |
| 17       | 0.689        | 1.333        | 1.740        | 2.110         | 2.567        | 2.898          | 3.646          |
| 18       | 0.688        | 1.330        | 1.734        | 2.101         | 2.552        | 2.878          | 3.610          |
| 19       | 0.688        | 1.328        | 1.729        | 2.093         | 2.539        | 2.861          | 3.579          |
| 20       | 0.687        | 1.325        | 1.725        | 2.086         | 2.528        | 2.845          | 3.552          |
| 21       | 0.686        | 1.323        | 1.721        | 2.080         | 2.518        | 2.831          | 3.527          |
| 22       | 0.686        | 1.321        | 1.717        | 2.074         | 2.508        | 2.819          | 3.505          |
| 23       | 0.685        | 1.319        | 1.714        | 2.069         | 2.500        | 2.807          | 3.485          |
| 24       | 0.685        | 1.318        | 1.711        | 2.064         | 2.492        | 2.797          | 3.467          |
| 25       | 0.684        | 1.316        | 1.708        | 2.060         | 2.485        | 2.787          | 3.450          |
| 26       | 0.684        | 1.315        | 1.706        | 2.056         | 2.479        | 2.779          | 3.435          |
| 27       | 0.684        | 1.314        | 1.703        | 2.052         | 2.473        | 2.771          | 3.421          |
| 28       | 0.683        | 1.313        | 1.701        | 2.048         | 2.467        | 2.763          | 3.408          |
| 29       | 0.683        | 1.311        | 1.699        | 2.045         | 2.462        | 2.756          | 3.396          |
| 30       | 0.683        | 1.310        | 1.697        | 2.042         | 2.457        | 2.750          | 3.385          |
| 40       | 0.681        | 1.303        | 1.684        | 2.021         | 2.423        | 2.704          | 3.307          |
| 60       | 0.679        | 1.296        | 1.671        | 2.000         | 2.390        | 2.660          | 3.232          |
| 120      | 0.677        | 1.289        | 1.658        | 1.980         | 2.358        | 2.617          | 3.160          |
| ∞        | 0.674        | 1.282        | 1.645        | 1.960         | 2.326        | 2.576          | 3.090          |

Note: The smaller probability shown at the head of each column is the area in one tail; the larger probability is the area in both tails.

TABLE D.3 Upper Percentage Points of the F Distribution

Example

- $\Pr(F > 1.59) = 0.25$
- $\Pr(F > 2.42) = 0.10$  for  $df N_1 = 10$
- $\Pr(F > 3.14) = 0.05$  and  $N_2 = 9$
- $\Pr(F > 5.26) = 0.01$



| df for denominator $N_2$ | Pr  | df for numerator $N_1$ |      |      |      |      |      |      |      |      |      |      |      |
|--------------------------|-----|------------------------|------|------|------|------|------|------|------|------|------|------|------|
|                          |     | 1                      | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   | 11   | 12   |
| 1                        | .25 | 5.83                   | 7.50 | 8.20 | 8.58 | 8.82 | 8.98 | 9.10 | 9.19 | 9.26 | 9.32 | 9.36 | 9.41 |
|                          | .10 | 39.9                   | 49.5 | 53.6 | 55.8 | 57.2 | 58.2 | 58.9 | 59.4 | 59.9 | 60.2 | 60.5 | 60.7 |
|                          | .05 | 161                    | 200  | 216  | 225  | 230  | 234  | 237  | 239  | 241  | 242  | 243  | 244  |
|                          | .01 |                        |      |      |      |      |      |      |      |      |      |      |      |
| 2                        | .25 | 2.57                   | 3.00 | 3.15 | 3.23 | 3.28 | 3.31 | 3.34 | 3.35 | 3.37 | 3.38 | 3.39 | 3.39 |
|                          | .10 | 8.53                   | 9.00 | 9.16 | 9.24 | 9.29 | 9.33 | 9.35 | 9.37 | 9.38 | 9.39 | 9.40 | 9.41 |
|                          | .05 | 18.5                   | 19.0 | 19.2 | 19.2 | 19.3 | 19.3 | 19.4 | 19.4 | 19.4 | 19.4 | 19.4 | 19.4 |
|                          | .01 | 98.5                   | 99.0 | 99.2 | 99.2 | 99.3 | 99.3 | 99.4 | 99.4 | 99.4 | 99.4 | 99.4 | 99.4 |
| 3                        | .25 | 2.02                   | 2.28 | 2.36 | 2.39 | 2.41 | 2.42 | 2.43 | 2.44 | 2.44 | 2.44 | 2.45 | 2.45 |
|                          | .10 | 5.54                   | 5.46 | 5.39 | 5.34 | 5.31 | 5.28 | 5.27 | 5.25 | 5.24 | 5.23 | 5.22 | 5.22 |
|                          | .05 | 10.1                   | 9.55 | 9.28 | 9.12 | 9.01 | 8.94 | 8.89 | 8.85 | 8.81 | 8.79 | 8.76 | 8.74 |
|                          | .01 | 34.1                   | 30.8 | 29.5 | 28.7 | 28.2 | 27.9 | 27.7 | 27.5 | 27.3 | 27.2 | 27.1 | 27.1 |
| 4                        | .25 | 1.81                   | 2.00 | 2.05 | 2.06 | 2.07 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 |
|                          | .10 | 4.54                   | 4.32 | 4.19 | 4.11 | 4.05 | 4.01 | 3.98 | 3.95 | 3.94 | 3.92 | 3.91 | 3.90 |
|                          | .05 | 7.71                   | 6.94 | 6.59 | 6.39 | 6.26 | 6.16 | 6.09 | 6.04 | 6.00 | 5.96 | 5.94 | 5.91 |
|                          | .01 | 21.2                   | 18.0 | 16.7 | 16.0 | 15.5 | 15.2 | 15.0 | 14.8 | 14.7 | 14.5 | 14.4 | 14.4 |
| 5                        | .25 | 1.69                   | 1.85 | 1.88 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
|                          | .10 | 4.06                   | 3.78 | 3.62 | 3.52 | 3.45 | 3.40 | 3.37 | 3.34 | 3.32 | 3.30 | 3.28 | 3.27 |
|                          | .05 | 6.61                   | 5.79 | 5.41 | 5.19 | 5.05 | 4.95 | 4.88 | 4.82 | 4.77 | 4.74 | 4.71 | 4.68 |
|                          | .01 | 16.3                   | 13.3 | 12.1 | 11.4 | 11.0 | 10.7 | 10.5 | 10.3 | 10.2 | 10.1 | 9.96 | 9.89 |
| 6                        | .25 | 1.62                   | 1.76 | 1.78 | 1.79 | 1.79 | 1.78 | 1.78 | 1.78 | 1.77 | 1.77 | 1.77 | 1.77 |
|                          | .10 | 3.78                   | 3.46 | 3.29 | 3.18 | 3.11 | 3.05 | 3.01 | 2.98 | 2.96 | 2.94 | 2.92 | 2.90 |
|                          | .05 | 5.99                   | 5.14 | 4.76 | 4.53 | 4.39 | 4.28 | 4.21 | 4.15 | 4.10 | 4.06 | 4.03 | 4.00 |
|                          | .01 | 13.7                   | 10.9 | 9.78 | 9.15 | 8.75 | 8.47 | 8.26 | 8.10 | 7.98 | 7.87 | 7.79 | 7.72 |
| 7                        | .25 | 1.57                   | 1.70 | 1.72 | 1.72 | 1.71 | 1.71 | 1.70 | 1.70 | 1.69 | 1.69 | 1.69 | 1.68 |
|                          | .10 | 3.59                   | 3.26 | 3.07 | 2.96 | 2.88 | 2.83 | 2.78 | 2.75 | 2.72 | 2.70 | 2.68 | 2.67 |
|                          | .05 | 5.59                   | 4.74 | 4.35 | 4.12 | 3.97 | 3.87 | 3.79 | 3.73 | 3.68 | 3.64 | 3.60 | 3.57 |
|                          | .01 | 12.2                   | 9.55 | 8.45 | 7.85 | 7.46 | 7.19 | 6.99 | 6.84 | 6.72 | 6.62 | 6.54 | 6.47 |
| 8                        | .25 | 1.54                   | 1.66 | 1.67 | 1.66 | 1.66 | 1.65 | 1.64 | 1.64 | 1.63 | 1.63 | 1.63 | 1.62 |
|                          | .10 | 3.46                   | 3.11 | 2.92 | 2.81 | 2.73 | 2.67 | 2.62 | 2.59 | 2.56 | 2.54 | 2.52 | 2.50 |
|                          | .05 | 5.32                   | 4.46 | 4.07 | 3.84 | 3.69 | 3.58 | 3.50 | 3.44 | 3.39 | 3.35 | 3.31 | 3.28 |
|                          | .01 | 11.3                   | 8.65 | 7.59 | 7.01 | 6.63 | 6.37 | 6.18 | 6.03 | 5.91 | 5.81 | 5.73 | 5.67 |
| 9                        | .25 | 1.51                   | 1.62 | 1.63 | 1.63 | 1.62 | 1.61 | 1.60 | 1.60 | 1.59 | 1.59 | 1.58 | 1.58 |
|                          | .10 | 3.36                   | 3.01 | 2.81 | 2.69 | 2.61 | 2.55 | 2.51 | 2.47 | 2.44 | 2.42 | 2.40 | 2.38 |
|                          | .05 | 5.12                   | 4.26 | 3.86 | 3.63 | 3.48 | 3.37 | 3.29 | 3.23 | 3.18 | 3.14 | 3.10 | 3.07 |
|                          | .01 | 10.6                   | 8.02 | 6.99 | 6.42 | 6.06 | 5.80 | 5.61 | 5.47 | 5.35 | 5.26 | 5.18 | 5.11 |

Source: From E. S. Pearson and H. O. Hartley, eds., *Biometrika Tables for Statisticians*, vol. 1, 3rd ed., table 18, Cambridge University Press, New York, 1966. Reproduced by permission of the editors and trustees of *Biometrika*.

# F-table continued

| df for numerator $N_1$ |      |      |      |      |      |      |      |      |      |      |          |     | df for denominator $N_2$ |
|------------------------|------|------|------|------|------|------|------|------|------|------|----------|-----|--------------------------|
| 15                     | 20   | 24   | 30   | 40   | 50   | 60   | 100  | 120  | 200  | 500  | $\infty$ | Pr  |                          |
| 9.49                   | 9.58 | 9.63 | 9.67 | 9.71 | 9.74 | 9.76 | 9.78 | 9.80 | 9.82 | 9.84 | 9.85     | .25 |                          |
| 61.2                   | 61.7 | 62.0 | 62.3 | 62.5 | 62.7 | 62.8 | 63.0 | 63.1 | 63.2 | 63.3 | 63.3     | .10 | 1                        |
| 246                    | 248  | 249  | 250  | 251  | 252  | 252  | 253  | 253  | 254  | 254  | 254      | .05 |                          |
| 3.41                   | 3.43 | 3.43 | 3.44 | 3.45 | 3.45 | 3.46 | 3.47 | 3.47 | 3.48 | 3.48 | 3.48     | .25 |                          |
| 9.42                   | 9.44 | 9.45 | 9.46 | 9.47 | 9.47 | 9.47 | 9.48 | 9.48 | 9.49 | 9.49 | 9.49     | .10 | 2                        |
| 19.4                   | 19.4 | 19.5 | 19.5 | 19.5 | 19.5 | 19.5 | 19.5 | 19.5 | 19.5 | 19.5 | 19.5     | .05 |                          |
| 99.4                   | 99.4 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5 | 99.5     | .01 |                          |
| 2.46                   | 2.46 | 2.46 | 2.47 | 2.47 | 2.47 | 2.47 | 2.47 | 2.47 | 2.47 | 2.47 | 2.47     | .25 |                          |
| 5.20                   | 5.18 | 5.18 | 5.17 | 5.16 | 5.15 | 5.15 | 5.14 | 5.14 | 5.14 | 5.14 | 5.13     | .10 | 3                        |
| 8.70                   | 8.66 | 8.64 | 8.62 | 8.59 | 8.58 | 8.57 | 8.55 | 8.55 | 8.54 | 8.53 | 8.53     | .05 |                          |
| 26.9                   | 26.7 | 26.6 | 26.5 | 26.4 | 26.4 | 26.3 | 26.2 | 26.2 | 26.2 | 26.1 | 26.1     | .01 |                          |
| 2.08                   | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08     | .25 |                          |
| 3.87                   | 3.84 | 3.83 | 3.82 | 3.80 | 3.80 | 3.79 | 3.78 | 3.78 | 3.77 | 3.76 | 3.76     | .10 | 4                        |
| 5.86                   | 5.80 | 5.77 | 5.75 | 5.72 | 5.70 | 5.69 | 5.66 | 5.66 | 5.65 | 5.64 | 5.63     | .05 |                          |
| 14.2                   | 14.0 | 13.9 | 13.8 | 13.7 | 13.7 | 13.7 | 13.6 | 13.6 | 13.5 | 13.5 | 13.5     | .01 |                          |
| 1.89                   | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87     | .25 |                          |
| 3.24                   | 3.21 | 3.19 | 3.17 | 3.16 | 3.15 | 3.14 | 3.13 | 3.12 | 3.12 | 3.11 | 3.10     | .10 | 5                        |
| 4.62                   | 4.56 | 4.53 | 4.50 | 4.46 | 4.44 | 4.43 | 4.41 | 4.40 | 4.39 | 4.37 | 4.36     | .05 |                          |
| 9.72                   | 9.55 | 9.47 | 9.38 | 9.29 | 9.24 | 9.20 | 9.13 | 9.11 | 9.08 | 9.04 | 9.02     | .01 |                          |
| 1.76                   | 1.76 | 1.75 | 1.75 | 1.75 | 1.75 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74     | .25 |                          |
| 2.87                   | 2.84 | 2.82 | 2.80 | 2.78 | 2.77 | 2.76 | 2.75 | 2.74 | 2.73 | 2.73 | 2.72     | .10 | 6                        |
| 3.94                   | 3.87 | 3.84 | 3.81 | 3.77 | 3.75 | 3.74 | 3.71 | 3.70 | 3.69 | 3.68 | 3.67     | .05 |                          |
| 7.56                   | 7.40 | 7.31 | 7.23 | 7.14 | 7.09 | 7.06 | 6.99 | 6.97 | 6.93 | 6.90 | 6.88     | .01 |                          |
| 1.68                   | 1.67 | 1.67 | 1.66 | 1.66 | 1.66 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65     | .25 |                          |
| 2.63                   | 2.59 | 2.58 | 2.56 | 2.54 | 2.52 | 2.51 | 2.50 | 2.49 | 2.48 | 2.48 | 2.47     | .10 | 7                        |
| 3.51                   | 3.44 | 3.41 | 3.38 | 3.34 | 3.32 | 3.30 | 3.27 | 3.27 | 3.25 | 3.24 | 3.23     | .05 |                          |
| 6.31                   | 6.16 | 6.07 | 5.99 | 5.91 | 5.86 | 5.82 | 5.75 | 5.74 | 5.70 | 5.67 | 5.65     | .01 |                          |
| 1.62                   | 1.61 | 1.60 | 1.60 | 1.59 | 1.59 | 1.59 | 1.58 | 1.58 | 1.58 | 1.58 | 1.58     | .25 |                          |
| 2.46                   | 2.42 | 2.40 | 2.38 | 2.36 | 2.35 | 2.34 | 2.32 | 2.32 | 2.31 | 2.30 | 2.29     | .10 | 8                        |
| 3.22                   | 3.15 | 3.12 | 3.08 | 3.04 | 2.02 | 3.01 | 2.97 | 2.97 | 2.95 | 2.94 | 2.93     | .05 |                          |
| 5.52                   | 5.36 | 5.28 | 5.20 | 5.12 | 5.07 | 5.03 | 4.96 | 4.95 | 4.91 | 4.88 | 4.86     | .01 |                          |
| 1.57                   | 1.56 | 1.56 | 1.55 | 1.55 | 1.54 | 1.54 | 1.53 | 1.53 | 1.53 | 1.53 | 1.53     | .25 |                          |
| 2.34                   | 2.30 | 2.28 | 2.25 | 2.23 | 2.22 | 2.21 | 2.19 | 2.18 | 2.17 | 2.17 | 2.16     | .10 | 9                        |
| 3.01                   | 2.94 | 2.90 | 2.86 | 2.83 | 2.80 | 2.79 | 2.76 | 2.75 | 2.73 | 2.72 | 2.71     | .05 |                          |
| 4.96                   | 4.81 | 4.73 | 4.65 | 4.57 | 4.52 | 4.48 | 4.42 | 4.40 | 4.36 | 4.33 | 4.31     | .01 |                          |

(Continued)



TABLE D.3 Upper Percentage Points of the  $F$  Distribution (Continued)

| df for denominator<br>$N_2$ | Pr  | df for numerator $N_1$ |      |      |      |      |      |      |      |      |      |      |      |
|-----------------------------|-----|------------------------|------|------|------|------|------|------|------|------|------|------|------|
|                             |     | 1                      | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   | 11   | 12   |
| 10                          | .25 | 1.49                   | 1.60 | 1.60 | 1.59 | 1.59 | 1.58 | 1.57 | 1.56 | 1.56 | 1.55 | 1.55 | 1.54 |
|                             | .10 | 3.29                   | 2.92 | 2.73 | 2.61 | 2.52 | 2.46 | 2.41 | 2.38 | 2.35 | 2.32 | 2.30 | 2.28 |
|                             | .05 | 4.96                   | 4.10 | 3.71 | 3.48 | 3.33 | 3.22 | 3.14 | 3.07 | 3.02 | 2.98 | 2.94 | 2.91 |
|                             | .01 | 10.0                   | 7.56 | 6.55 | 5.99 | 5.64 | 5.39 | 5.20 | 5.06 | 4.94 | 4.85 | 4.77 | 4.71 |
| 11                          | .25 | 1.47                   | 1.58 | 1.58 | 1.57 | 1.56 | 1.55 | 1.54 | 1.53 | 1.53 | 1.52 | 1.52 | 1.51 |
|                             | .10 | 3.23                   | 2.86 | 2.66 | 2.54 | 2.45 | 2.39 | 2.34 | 2.30 | 2.27 | 2.25 | 2.23 | 2.21 |
|                             | .05 | 4.84                   | 3.98 | 3.59 | 3.36 | 3.20 | 3.09 | 3.01 | 2.95 | 2.90 | 2.85 | 2.82 | 2.79 |
|                             | .01 | 9.65                   | 7.21 | 6.22 | 5.67 | 5.32 | 5.07 | 4.89 | 4.74 | 4.63 | 4.54 | 4.46 | 4.40 |
| 12                          | .25 | 1.46                   | 1.56 | 1.56 | 1.55 | 1.54 | 1.53 | 1.52 | 1.51 | 1.51 | 1.50 | 1.50 | 1.49 |
|                             | .10 | 3.18                   | 2.81 | 2.61 | 2.48 | 2.39 | 2.33 | 2.28 | 2.24 | 2.21 | 2.19 | 2.17 | 2.15 |
|                             | .05 | 4.75                   | 3.89 | 3.49 | 3.26 | 3.11 | 3.00 | 2.91 | 2.85 | 2.80 | 2.75 | 2.72 | 2.69 |
|                             | .01 | 9.33                   | 6.93 | 5.95 | 5.41 | 5.06 | 4.82 | 4.64 | 4.50 | 4.39 | 4.30 | 4.22 | 4.16 |
| 13                          | .25 | 1.45                   | 1.55 | 1.55 | 1.53 | 1.52 | 1.51 | 1.50 | 1.49 | 1.49 | 1.48 | 1.47 | 1.47 |
|                             | .10 | 3.14                   | 2.76 | 2.56 | 2.43 | 2.35 | 2.28 | 2.23 | 2.20 | 2.16 | 2.14 | 2.12 | 2.10 |
|                             | .05 | 4.67                   | 3.81 | 3.41 | 3.18 | 3.03 | 2.92 | 2.83 | 2.77 | 2.71 | 2.67 | 2.63 | 2.60 |
|                             | .01 | 9.07                   | 6.70 | 5.74 | 5.21 | 4.86 | 4.62 | 4.44 | 4.30 | 4.19 | 4.10 | 4.02 | 3.96 |
| 14                          | .25 | 1.44                   | 1.53 | 1.53 | 1.52 | 1.51 | 1.50 | 1.49 | 1.48 | 1.47 | 1.46 | 1.46 | 1.45 |
|                             | .10 | 3.10                   | 2.73 | 2.52 | 2.39 | 2.31 | 2.24 | 2.19 | 2.15 | 2.12 | 2.10 | 2.08 | 2.05 |
|                             | .05 | 4.60                   | 3.74 | 3.34 | 3.11 | 2.96 | 2.85 | 2.76 | 2.70 | 2.65 | 2.60 | 2.57 | 2.53 |
|                             | .01 | 8.86                   | 6.51 | 5.56 | 5.04 | 4.69 | 4.46 | 4.28 | 4.14 | 4.03 | 3.94 | 3.86 | 3.80 |
| 15                          | .25 | 1.43                   | 1.52 | 1.52 | 1.51 | 1.49 | 1.48 | 1.47 | 1.46 | 1.46 | 1.45 | 1.44 | 1.44 |
|                             | .10 | 3.07                   | 2.70 | 2.49 | 2.36 | 2.27 | 2.21 | 2.16 | 2.12 | 2.09 | 2.06 | 2.04 | 2.02 |
|                             | .05 | 4.54                   | 3.68 | 3.29 | 3.06 | 2.90 | 2.79 | 2.71 | 2.64 | 2.59 | 2.54 | 2.51 | 2.48 |
|                             | .01 | 8.68                   | 6.36 | 5.42 | 4.89 | 4.56 | 4.32 | 4.14 | 4.00 | 3.89 | 3.80 | 3.73 | 3.67 |
| 16                          | .25 | 1.42                   | 1.51 | 1.51 | 1.50 | 1.48 | 1.47 | 1.46 | 1.45 | 1.44 | 1.44 | 1.44 | 1.43 |
|                             | .10 | 3.05                   | 2.67 | 2.46 | 2.33 | 2.24 | 2.18 | 2.13 | 2.09 | 2.06 | 2.03 | 2.01 | 1.99 |
|                             | .05 | 4.49                   | 3.63 | 3.24 | 3.01 | 2.85 | 2.74 | 2.66 | 2.59 | 2.54 | 2.49 | 2.46 | 2.42 |
|                             | .01 | 8.53                   | 6.23 | 5.29 | 4.77 | 4.44 | 4.20 | 4.03 | 3.89 | 3.78 | 3.69 | 3.62 | 3.55 |
| 17                          | .25 | 1.42                   | 1.51 | 1.50 | 1.49 | 1.47 | 1.46 | 1.45 | 1.44 | 1.43 | 1.43 | 1.42 | 1.41 |
|                             | .10 | 3.03                   | 2.64 | 2.44 | 2.31 | 2.22 | 2.15 | 2.10 | 2.06 | 2.03 | 2.00 | 1.98 | 1.96 |
|                             | .05 | 4.45                   | 3.59 | 3.20 | 2.96 | 2.81 | 2.70 | 2.61 | 2.55 | 2.49 | 2.45 | 2.41 | 2.38 |
|                             | .01 | 8.40                   | 6.11 | 5.18 | 4.67 | 4.34 | 4.10 | 3.93 | 3.79 | 3.68 | 3.59 | 3.52 | 3.46 |
| 18                          | .25 | 1.41                   | 1.50 | 1.49 | 1.48 | 1.46 | 1.45 | 1.44 | 1.43 | 1.42 | 1.42 | 1.41 | 1.40 |
|                             | .10 | 3.01                   | 2.62 | 2.42 | 2.29 | 2.20 | 2.13 | 2.08 | 2.04 | 2.00 | 1.98 | 1.96 | 1.93 |
|                             | .05 | 4.41                   | 3.55 | 3.16 | 2.93 | 2.77 | 2.66 | 2.58 | 2.51 | 2.46 | 2.41 | 2.37 | 2.34 |
|                             | .01 | 8.29                   | 6.01 | 5.09 | 4.58 | 4.25 | 4.01 | 3.84 | 3.71 | 3.60 | 3.51 | 3.43 | 3.37 |
| 19                          | .25 | 1.41                   | 1.49 | 1.49 | 1.47 | 1.46 | 1.44 | 1.43 | 1.42 | 1.41 | 1.41 | 1.40 | 1.40 |
|                             | .10 | 2.99                   | 2.61 | 2.40 | 2.27 | 2.18 | 2.11 | 2.06 | 2.02 | 1.98 | 1.96 | 1.94 | 1.91 |
|                             | .05 | 4.38                   | 3.52 | 3.13 | 2.90 | 2.74 | 2.63 | 2.54 | 2.48 | 2.42 | 2.38 | 2.34 | 2.31 |
|                             | .01 | 8.18                   | 5.93 | 5.01 | 4.50 | 4.17 | 3.94 | 3.77 | 3.63 | 3.52 | 3.43 | 3.36 | 3.30 |
| 20                          | .25 | 1.40                   | 1.49 | 1.48 | 1.46 | 1.45 | 1.44 | 1.43 | 1.42 | 1.41 | 1.40 | 1.39 | 1.39 |
|                             | .10 | 2.97                   | 2.59 | 2.38 | 2.25 | 2.16 | 2.09 | 2.04 | 2.00 | 1.96 | 1.94 | 1.92 | 1.89 |
|                             | .05 | 4.35                   | 3.49 | 3.10 | 2.87 | 2.71 | 2.60 | 2.51 | 2.45 | 2.39 | 2.35 | 2.31 | 2.28 |
|                             | .01 | 8.10                   | 5.85 | 4.94 | 4.43 | 4.10 | 3.87 | 3.70 | 3.56 | 3.46 | 3.37 | 3.29 | 3.23 |

F-table (continued)

| df for numerator $N_1$ |      |      |      |      |      |      |      |      |      |      |          |     | df for denominator $N_2$ |
|------------------------|------|------|------|------|------|------|------|------|------|------|----------|-----|--------------------------|
| 15                     | 20   | 24   | 30   | 40   | 50   | 60   | 100  | 120  | 200  | 500  | $\infty$ | Pr  | $N_2$                    |
| 1.53                   | 1.52 | 1.52 | 1.51 | 1.51 | 1.50 | 1.50 | 1.49 | 1.49 | 1.49 | 1.48 | 1.48     | .25 | 10                       |
| 2.24                   | 2.20 | 2.18 | 2.16 | 2.13 | 2.12 | 2.11 | 2.09 | 2.08 | 2.07 | 2.06 | 2.06     | .10 | 10                       |
| 2.85                   | 2.77 | 2.74 | 2.70 | 2.66 | 2.64 | 2.62 | 2.59 | 2.58 | 2.56 | 2.55 | 2.54     | .05 | 10                       |
| 4.56                   | 4.41 | 4.33 | 4.25 | 4.17 | 4.12 | 4.08 | 4.01 | 4.00 | 3.96 | 3.93 | 3.91     | .01 | 10                       |
| 1.50                   | 1.49 | 1.49 | 1.48 | 1.47 | 1.47 | 1.47 | 1.46 | 1.46 | 1.46 | 1.45 | 1.45     | .25 | 11                       |
| 2.17                   | 2.12 | 2.10 | 2.08 | 2.05 | 2.04 | 2.03 | 2.00 | 2.00 | 1.99 | 1.98 | 1.97     | .10 | 11                       |
| 2.72                   | 2.65 | 2.61 | 2.57 | 2.53 | 2.51 | 2.49 | 2.46 | 2.45 | 2.43 | 2.42 | 2.40     | .05 | 11                       |
| 4.25                   | 4.10 | 4.02 | 3.94 | 3.86 | 3.81 | 3.78 | 3.71 | 3.69 | 3.66 | 3.62 | 3.60     | .01 | 11                       |
| 1.48                   | 1.47 | 1.46 | 1.45 | 1.45 | 1.44 | 1.44 | 1.43 | 1.43 | 1.43 | 1.42 | 1.42     | .25 | 12                       |
| 2.10                   | 2.06 | 2.04 | 2.01 | 1.99 | 1.97 | 1.96 | 1.94 | 1.93 | 1.92 | 1.91 | 1.90     | .10 | 12                       |
| 2.62                   | 2.54 | 2.51 | 2.47 | 2.43 | 2.40 | 2.38 | 2.35 | 2.34 | 2.32 | 2.31 | 2.30     | .05 | 12                       |
| 4.01                   | 3.86 | 3.78 | 3.70 | 3.62 | 3.57 | 3.54 | 3.47 | 3.45 | 3.41 | 3.38 | 3.36     | .01 | 12                       |
| 1.46                   | 1.45 | 1.44 | 1.43 | 1.42 | 1.42 | 1.42 | 1.41 | 1.41 | 1.40 | 1.40 | 1.40     | .25 | 13                       |
| 2.05                   | 2.01 | 1.98 | 1.96 | 1.93 | 1.92 | 1.90 | 1.88 | 1.88 | 1.86 | 1.85 | 1.85     | .10 | 13                       |
| 2.53                   | 2.46 | 2.42 | 2.38 | 2.34 | 2.31 | 2.30 | 2.26 | 2.25 | 2.23 | 2.22 | 2.21     | .05 | 13                       |
| 3.82                   | 3.66 | 3.59 | 3.51 | 3.43 | 3.38 | 3.34 | 3.27 | 3.25 | 3.22 | 3.19 | 3.17     | .01 | 13                       |
| 1.44                   | 1.43 | 1.42 | 1.41 | 1.41 | 1.40 | 1.40 | 1.39 | 1.39 | 1.39 | 1.38 | 1.38     | .25 | 14                       |
| 2.01                   | 1.96 | 1.94 | 1.91 | 1.89 | 1.87 | 1.86 | 1.83 | 1.83 | 1.82 | 1.80 | 1.80     | .10 | 14                       |
| 2.46                   | 2.39 | 2.35 | 2.31 | 2.27 | 2.24 | 2.22 | 2.19 | 2.18 | 2.16 | 2.14 | 2.13     | .05 | 14                       |
| 3.66                   | 3.51 | 3.43 | 3.35 | 3.27 | 3.22 | 3.18 | 3.11 | 3.09 | 3.06 | 3.03 | 3.00     | .01 | 14                       |
| 1.43                   | 1.41 | 1.41 | 1.40 | 1.39 | 1.39 | 1.38 | 1.38 | 1.37 | 1.37 | 1.36 | 1.36     | .25 | 15                       |
| 1.97                   | 1.92 | 1.90 | 1.87 | 1.85 | 1.83 | 1.82 | 1.79 | 1.79 | 1.77 | 1.76 | 1.76     | .10 | 15                       |
| 2.40                   | 2.33 | 2.29 | 2.25 | 2.20 | 2.18 | 2.16 | 2.12 | 2.11 | 2.10 | 2.08 | 2.07     | .05 | 15                       |
| 3.52                   | 3.37 | 3.29 | 3.21 | 3.13 | 3.08 | 3.05 | 2.98 | 2.96 | 2.92 | 2.89 | 2.87     | .01 | 15                       |
| 1.41                   | 1.40 | 1.39 | 1.38 | 1.37 | 1.37 | 1.36 | 1.36 | 1.35 | 1.35 | 1.34 | 1.34     | .25 | 16                       |
| 1.94                   | 1.89 | 1.87 | 1.84 | 1.81 | 1.79 | 1.78 | 1.76 | 1.75 | 1.74 | 1.73 | 1.72     | .10 | 16                       |
| 2.35                   | 2.28 | 2.24 | 2.19 | 2.15 | 2.12 | 2.11 | 2.07 | 2.06 | 2.04 | 2.02 | 2.01     | .05 | 16                       |
| 3.41                   | 3.26 | 3.18 | 3.10 | 3.02 | 2.97 | 2.93 | 2.86 | 2.84 | 2.81 | 2.78 | 2.75     | .01 | 16                       |
| 1.40                   | 1.39 | 1.38 | 1.37 | 1.36 | 1.35 | 1.35 | 1.34 | 1.34 | 1.34 | 1.33 | 1.33     | .25 | 17                       |
| 1.91                   | 1.86 | 1.84 | 1.81 | 1.78 | 1.76 | 1.75 | 1.73 | 1.72 | 1.71 | 1.69 | 1.69     | .10 | 17                       |
| 2.31                   | 2.23 | 2.19 | 2.15 | 2.10 | 2.08 | 2.06 | 2.02 | 2.01 | 1.99 | 1.97 | 1.96     | .05 | 17                       |
| 3.31                   | 3.16 | 3.08 | 3.00 | 2.92 | 2.87 | 2.83 | 2.76 | 2.75 | 2.71 | 2.68 | 2.65     | .01 | 17                       |
| 1.39                   | 1.38 | 1.37 | 1.36 | 1.35 | 1.34 | 1.34 | 1.33 | 1.33 | 1.32 | 1.32 | 1.32     | .25 | 18                       |
| 1.89                   | 1.84 | 1.81 | 1.78 | 1.75 | 1.74 | 1.72 | 1.70 | 1.69 | 1.68 | 1.67 | 1.66     | .10 | 18                       |
| 2.27                   | 2.19 | 2.15 | 2.11 | 2.06 | 2.04 | 2.02 | 1.98 | 1.97 | 1.95 | 1.93 | 1.92     | .05 | 18                       |
| 3.23                   | 3.08 | 3.00 | 2.92 | 2.84 | 2.78 | 2.75 | 2.68 | 2.66 | 2.62 | 2.59 | 2.57     | .01 | 18                       |
| 1.38                   | 1.37 | 1.36 | 1.35 | 1.34 | 1.33 | 1.33 | 1.32 | 1.32 | 1.31 | 1.31 | 1.30     | .25 | 19                       |
| 1.86                   | 1.81 | 1.79 | 1.76 | 1.73 | 1.71 | 1.70 | 1.67 | 1.67 | 1.65 | 1.64 | 1.63     | .10 | 19                       |
| 2.23                   | 2.16 | 2.11 | 2.07 | 2.03 | 2.00 | 1.98 | 1.94 | 1.93 | 1.91 | 1.89 | 1.88     | .05 | 19                       |
| 3.15                   | 3.00 | 2.92 | 2.84 | 2.76 | 2.71 | 2.67 | 2.60 | 2.58 | 2.55 | 2.51 | 2.49     | .01 | 19                       |
| 1.37                   | 1.36 | 1.35 | 1.34 | 1.33 | 1.33 | 1.32 | 1.31 | 1.31 | 1.30 | 1.30 | 1.29     | .25 | 20                       |
| 1.84                   | 1.79 | 1.77 | 1.74 | 1.71 | 1.69 | 1.68 | 1.65 | 1.64 | 1.63 | 1.62 | 1.61     | .10 | 20                       |
| 2.20                   | 2.12 | 2.08 | 2.04 | 1.99 | 1.97 | 1.95 | 1.91 | 1.90 | 1.88 | 1.86 | 1.84     | .05 | 20                       |
| 3.09                   | 2.94 | 2.86 | 2.78 | 2.69 | 2.64 | 2.61 | 2.54 | 2.52 | 2.48 | 2.44 | 2.42     | .01 | 20                       |

(Continues)

TABLE D.3 Upper Percentage Points of the *F* Distribution (Continued)

| df for denominator<br>$N_2$ | df for numerator $N_1$ |      |      |      |      |      |      |      |      |      |      |      |      |
|-----------------------------|------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
|                             | Pr                     | 1    | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   | 11   | 12   |
| 22                          | .25                    | 1.40 | 1.48 | 1.47 | 1.45 | 1.44 | 1.42 | 1.41 | 1.40 | 1.39 | 1.39 | 1.38 | 1.37 |
|                             | .10                    | 2.95 | 2.56 | 2.35 | 2.22 | 2.13 | 2.06 | 2.01 | 1.97 | 1.93 | 1.90 | 1.88 | 1.86 |
|                             | .05                    | 4.30 | 3.44 | 3.05 | 2.82 | 2.66 | 2.55 | 2.46 | 2.40 | 2.34 | 2.30 | 2.26 | 2.23 |
|                             | .01                    | 7.95 | 5.72 | 4.82 | 4.31 | 3.99 | 3.76 | 3.59 | 3.45 | 3.35 | 3.26 | 3.18 | 3.12 |
| 24                          | .25                    | 1.39 | 1.47 | 1.46 | 1.44 | 1.43 | 1.41 | 1.40 | 1.39 | 1.38 | 1.38 | 1.37 | 1.36 |
|                             | .10                    | 2.93 | 2.54 | 2.33 | 2.19 | 2.10 | 2.04 | 1.98 | 1.94 | 1.91 | 1.88 | 1.85 | 1.83 |
|                             | .05                    | 4.26 | 3.40 | 3.01 | 2.78 | 2.62 | 2.51 | 2.42 | 2.36 | 2.30 | 2.25 | 2.21 | 2.18 |
|                             | .01                    | 7.82 | 5.61 | 4.72 | 4.22 | 3.90 | 3.67 | 3.50 | 3.36 | 3.26 | 3.17 | 3.09 | 3.03 |
| 26                          | .25                    | 1.38 | 1.46 | 1.45 | 1.44 | 1.42 | 1.41 | 1.39 | 1.38 | 1.37 | 1.37 | 1.36 | 1.35 |
|                             | .10                    | 2.91 | 2.52 | 2.31 | 2.17 | 2.08 | 2.01 | 1.96 | 1.92 | 1.88 | 1.86 | 1.84 | 1.81 |
|                             | .05                    | 4.23 | 3.37 | 2.98 | 2.74 | 2.59 | 2.47 | 2.39 | 2.32 | 2.27 | 2.22 | 2.18 | 2.15 |
|                             | .01                    | 7.72 | 5.53 | 4.64 | 4.14 | 3.82 | 3.59 | 3.42 | 3.29 | 3.18 | 3.09 | 3.02 | 2.96 |
| 28                          | .25                    | 1.38 | 1.46 | 1.45 | 1.43 | 1.41 | 1.40 | 1.39 | 1.38 | 1.37 | 1.36 | 1.35 | 1.34 |
|                             | .10                    | 2.89 | 2.50 | 2.29 | 2.16 | 2.06 | 2.00 | 1.94 | 1.90 | 1.87 | 1.84 | 1.81 | 1.79 |
|                             | .05                    | 4.20 | 3.34 | 2.95 | 2.71 | 2.56 | 2.45 | 2.36 | 2.29 | 2.24 | 2.19 | 2.15 | 2.12 |
|                             | .01                    | 7.64 | 5.45 | 4.57 | 4.07 | 3.75 | 3.53 | 3.36 | 3.23 | 3.12 | 3.03 | 2.96 | 2.90 |
| 30                          | .25                    | 1.38 | 1.45 | 1.44 | 1.42 | 1.41 | 1.39 | 1.38 | 1.37 | 1.36 | 1.35 | 1.35 | 1.34 |
|                             | .10                    | 2.88 | 2.49 | 2.28 | 2.14 | 2.05 | 1.98 | 1.93 | 1.88 | 1.85 | 1.82 | 1.79 | 1.77 |
|                             | .05                    | 4.17 | 3.32 | 2.92 | 2.69 | 2.53 | 2.42 | 2.33 | 2.27 | 2.21 | 2.16 | 2.13 | 2.09 |
|                             | .01                    | 7.56 | 5.39 | 4.51 | 4.02 | 3.70 | 3.47 | 3.30 | 3.17 | 3.07 | 2.98 | 2.91 | 2.84 |
| 40                          | .25                    | 1.36 | 1.44 | 1.42 | 1.40 | 1.39 | 1.37 | 1.36 | 1.35 | 1.34 | 1.33 | 1.32 | 1.31 |
|                             | .10                    | 2.84 | 2.44 | 2.23 | 2.09 | 2.00 | 1.93 | 1.87 | 1.83 | 1.79 | 1.76 | 1.73 | 1.71 |
|                             | .05                    | 4.08 | 3.23 | 2.84 | 2.61 | 2.45 | 2.34 | 2.25 | 2.18 | 2.12 | 2.08 | 2.04 | 2.00 |
|                             | .01                    | 7.31 | 5.18 | 4.31 | 3.83 | 3.51 | 3.29 | 3.12 | 2.99 | 2.89 | 2.80 | 2.73 | 2.66 |
| 60                          | .25                    | 1.35 | 1.42 | 1.41 | 1.38 | 1.37 | 1.35 | 1.33 | 1.32 | 1.31 | 1.30 | 1.29 | 1.29 |
|                             | .10                    | 2.79 | 2.39 | 2.18 | 2.04 | 1.95 | 1.87 | 1.82 | 1.77 | 1.74 | 1.71 | 1.68 | 1.66 |
|                             | .05                    | 4.00 | 3.15 | 2.76 | 2.53 | 2.37 | 2.25 | 2.17 | 2.10 | 2.04 | 1.99 | 1.95 | 1.92 |
|                             | .01                    | 7.08 | 4.98 | 4.13 | 3.65 | 3.34 | 3.12 | 2.95 | 2.82 | 2.72 | 2.63 | 2.56 | 2.50 |
| 120                         | .25                    | 1.34 | 1.40 | 1.39 | 1.37 | 1.35 | 1.33 | 1.31 | 1.30 | 1.29 | 1.28 | 1.27 | 1.26 |
|                             | .10                    | 2.75 | 2.35 | 2.13 | 1.99 | 1.90 | 1.82 | 1.77 | 1.72 | 1.68 | 1.65 | 1.62 | 1.60 |
|                             | .05                    | 3.92 | 3.07 | 2.68 | 2.45 | 2.29 | 2.17 | 2.09 | 2.02 | 1.96 | 1.91 | 1.87 | 1.83 |
|                             | .01                    | 6.85 | 4.79 | 3.95 | 3.48 | 3.17 | 2.96 | 2.79 | 2.66 | 2.56 | 2.47 | 2.40 | 2.34 |
| 200                         | .25                    | 1.33 | 1.39 | 1.38 | 1.36 | 1.34 | 1.32 | 1.31 | 1.29 | 1.28 | 1.27 | 1.26 | 1.25 |
|                             | .10                    | 2.73 | 2.33 | 2.11 | 1.97 | 1.88 | 1.80 | 1.75 | 1.70 | 1.66 | 1.63 | 1.60 | 1.57 |
|                             | .05                    | 3.89 | 3.04 | 2.65 | 2.42 | 2.26 | 2.14 | 2.06 | 1.98 | 1.93 | 1.88 | 1.84 | 1.80 |
|                             | .01                    | 6.76 | 4.71 | 3.88 | 3.41 | 3.11 | 2.89 | 2.73 | 2.60 | 2.50 | 2.41 | 2.34 | 2.27 |
| $\infty$                    | .25                    | 1.32 | 1.39 | 1.37 | 1.35 | 1.33 | 1.31 | 1.29 | 1.28 | 1.27 | 1.25 | 1.24 | 1.24 |
|                             | .10                    | 2.71 | 2.30 | 2.08 | 1.94 | 1.85 | 1.77 | 1.72 | 1.67 | 1.63 | 1.60 | 1.57 | 1.55 |
|                             | .05                    | 3.84 | 3.00 | 2.60 | 2.37 | 2.21 | 2.10 | 2.01 | 1.94 | 1.88 | 1.83 | 1.79 | 1.75 |
|                             | .01                    | 6.63 | 4.61 | 3.78 | 3.32 | 3.02 | 2.80 | 2.64 | 2.51 | 2.41 | 2.32 | 2.25 | 2.18 |

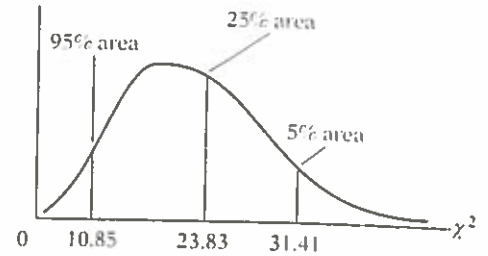
F-table continued

|                                 |      |      |      |      |      |      |      |      |      |      |      |     | df for<br>denom-<br>inator<br>N <sub>2</sub> |
|---------------------------------|------|------|------|------|------|------|------|------|------|------|------|-----|--|
|                                 |      |      |      |      |      |      |      |      |      |      |      |     | Pr   |
| df for numerator N <sub>1</sub> |      |      |      |      |      |      |      |      |      |      |      |     |  |
| 15                              | 20   | 24   | 30   | 40   | 50   | 60   | 100  | 120  | 200  | 500  | ∞    |     |  |
| 1.36                            | 1.34 | 1.33 | 1.32 | 1.31 | 1.31 | 1.30 | 1.30 | 1.30 | 1.29 | 1.29 | 1.28 | .25 |  |
| 1.81                            | 1.76 | 1.73 | 1.70 | 1.67 | 1.65 | 1.64 | 1.61 | 1.60 | 1.59 | 1.58 | 1.57 | .10 | 22   |
| 2.15                            | 2.07 | 2.03 | 1.98 | 1.94 | 1.91 | 1.89 | 1.85 | 1.84 | 1.82 | 1.80 | 1.78 | .05 |  |
| 2.98                            | 2.83 | 2.75 | 2.67 | 2.58 | 2.53 | 2.50 | 2.42 | 2.40 | 2.36 | 2.33 | 2.31 | .01 |  |
| 1.35                            | 1.33 | 1.32 | 1.31 | 1.30 | 1.29 | 1.29 | 1.28 | 1.28 | 1.27 | 1.27 | 1.26 | .25 |  |
| 1.78                            | 1.73 | 1.70 | 1.67 | 1.64 | 1.62 | 1.61 | 1.58 | 1.57 | 1.56 | 1.54 | 1.53 | .10 | 24   |
| 2.11                            | 2.03 | 1.98 | 1.94 | 1.89 | 1.86 | 1.84 | 1.80 | 1.79 | 1.77 | 1.75 | 1.73 | .05 |  |
| 2.89                            | 2.74 | 2.66 | 2.58 | 2.49 | 2.44 | 2.40 | 2.33 | 2.31 | 2.27 | 2.24 | 2.21 | .01 |  |
| 1.34                            | 1.32 | 1.31 | 1.30 | 1.29 | 1.28 | 1.28 | 1.26 | 1.26 | 1.26 | 1.25 | 1.25 | .25 |  |
| 1.76                            | 1.71 | 1.68 | 1.65 | 1.61 | 1.59 | 1.58 | 1.55 | 1.54 | 1.53 | 1.51 | 1.50 | .10 | 26   |
| 2.07                            | 1.99 | 1.95 | 1.90 | 1.85 | 1.82 | 1.80 | 1.76 | 1.75 | 1.73 | 1.71 | 1.69 | .05 |  |
| 2.81                            | 2.66 | 2.58 | 2.50 | 2.42 | 2.36 | 2.33 | 2.25 | 2.23 | 2.19 | 2.16 | 2.13 | .01 |  |
| 1.33                            | 1.31 | 1.30 | 1.29 | 1.28 | 1.27 | 1.27 | 1.26 | 1.25 | 1.25 | 1.24 | 1.24 | .25 |  |
| 1.74                            | 1.69 | 1.66 | 1.63 | 1.59 | 1.57 | 1.56 | 1.53 | 1.52 | 1.50 | 1.49 | 1.48 | .10 | 28   |
| 2.04                            | 1.96 | 1.91 | 1.87 | 1.82 | 1.79 | 1.77 | 1.73 | 1.71 | 1.69 | 1.67 | 1.65 | .05 |  |
| 2.75                            | 2.60 | 2.52 | 2.44 | 2.35 | 2.30 | 2.26 | 2.19 | 2.17 | 2.13 | 2.09 | 2.06 | .01 |  |
| 1.32                            | 1.30 | 1.29 | 1.28 | 1.27 | 1.26 | 1.26 | 1.25 | 1.24 | 1.24 | 1.23 | 1.23 | .25 |  |
| 1.72                            | 1.67 | 1.64 | 1.61 | 1.57 | 1.55 | 1.54 | 1.51 | 1.50 | 1.48 | 1.47 | 1.46 | .10 | 30   |
| 2.01                            | 1.93 | 1.89 | 1.84 | 1.79 | 1.76 | 1.74 | 1.70 | 1.68 | 1.66 | 1.64 | 1.62 | .05 |  |
| 2.70                            | 2.55 | 2.47 | 2.39 | 2.30 | 2.25 | 2.21 | 2.13 | 2.11 | 2.07 | 2.03 | 2.01 | .01 |  |
| 1.30                            | 1.28 | 1.26 | 1.25 | 1.24 | 1.23 | 1.22 | 1.21 | 1.21 | 1.20 | 1.19 | 1.19 | .25 |  |
| 1.66                            | 1.61 | 1.57 | 1.54 | 1.51 | 1.48 | 1.47 | 1.43 | 1.42 | 1.41 | 1.39 | 1.38 | .10 | 40   |
| 1.92                            | 1.84 | 1.79 | 1.74 | 1.69 | 1.66 | 1.64 | 1.59 | 1.58 | 1.55 | 1.53 | 1.51 | .05 |  |
| 2.52                            | 2.37 | 2.29 | 2.20 | 2.11 | 2.06 | 2.02 | 1.94 | 1.92 | 1.87 | 1.83 | 1.80 | .01 |  |
| 1.27                            | 1.25 | 1.24 | 1.22 | 1.21 | 1.20 | 1.19 | 1.17 | 1.17 | 1.16 | 1.15 | 1.15 | .25 |  |
| 1.60                            | 1.54 | 1.51 | 1.48 | 1.44 | 1.41 | 1.40 | 1.36 | 1.35 | 1.33 | 1.31 | 1.29 | .10 | 60   |
| 1.84                            | 1.75 | 1.70 | 1.65 | 1.59 | 1.56 | 1.53 | 1.48 | 1.47 | 1.44 | 1.41 | 1.39 | .05 |  |
| 2.35                            | 2.20 | 2.12 | 2.03 | 1.94 | 1.88 | 1.84 | 1.75 | 1.73 | 1.68 | 1.63 | 1.60 | .01 |  |
| 1.24                            | 1.22 | 1.21 | 1.19 | 1.18 | 1.17 | 1.16 | 1.14 | 1.13 | 1.12 | 1.11 | 1.10 | .25 |  |
| 1.55                            | 1.48 | 1.45 | 1.41 | 1.37 | 1.34 | 1.32 | 1.27 | 1.26 | 1.24 | 1.21 | 1.19 | .10 | 120  |
| 1.75                            | 1.66 | 1.61 | 1.55 | 1.50 | 1.46 | 1.43 | 1.37 | 1.35 | 1.32 | 1.28 | 1.25 | .05 |  |
| 2.19                            | 2.03 | 1.95 | 1.86 | 1.76 | 1.70 | 1.66 | 1.56 | 1.53 | 1.48 | 1.42 | 1.38 | .01 |  |
| 1.23                            | 1.21 | 1.20 | 1.18 | 1.16 | 1.14 | 1.12 | 1.11 | 1.10 | 1.09 | 1.08 | 1.06 | .25 |  |
| 1.52                            | 1.46 | 1.42 | 1.38 | 1.34 | 1.31 | 1.28 | 1.24 | 1.22 | 1.20 | 1.17 | 1.14 | .10 | 200  |
| 1.72                            | 1.62 | 1.57 | 1.52 | 1.46 | 1.41 | 1.39 | 1.32 | 1.29 | 1.26 | 1.22 | 1.19 | .05 |  |
| 2.13                            | 1.97 | 1.89 | 1.79 | 1.69 | 1.63 | 1.58 | 1.48 | 1.44 | 1.39 | 1.33 | 1.28 | .01 |  |
| 1.22                            | 1.19 | 1.18 | 1.16 | 1.14 | 1.13 | 1.12 | 1.09 | 1.08 | 1.07 | 1.04 | 1.00 | .25 |  |
| 1.49                            | 1.42 | 1.38 | 1.34 | 1.30 | 1.26 | 1.24 | 1.18 | 1.17 | 1.13 | 1.08 | 1.00 | .10 | ∞  |
| 1.67                            | 1.57 | 1.52 | 1.46 | 1.39 | 1.35 | 1.32 | 1.24 | 1.22 | 1.17 | 1.11 | 1.00 | .05 |  |
| 2.04                            | 1.88 | 1.79 | 1.70 | 1.59 | 1.52 | 1.47 | 1.36 | 1.32 | 1.25 | 1.15 | 1.00 | .01 |  |

**TABLE D.4**  
Upper Percentage  
Points of the  $\chi^2$   
Distribution

**Example**

$\Pr(\chi^2 > 10.85) = 0.95$   
 $\Pr(\chi^2 > 23.83) = 0.25$   
 $\Pr(\chi^2 > 31.41) = 0.05$   
 for  $df = 20$



| Degrees of freedom \ Pr | .995                     | .990                    | .975                    | .950                    | .900     |
|-------------------------|--------------------------|-------------------------|-------------------------|-------------------------|----------|
| 1                       | $392704 \times 10^{-10}$ | $157088 \times 10^{-9}$ | $982069 \times 10^{-9}$ | $393214 \times 10^{-8}$ | .0157908 |
| 2                       | .0100251                 | .0201007                | .0506356                | .102587                 | .210720  |
| 3                       | .0717212                 | .114832                 | .215795                 | .351846                 | .584375  |
| 4                       | .206990                  | .297110                 | .484419                 | .710721                 | 1.063623 |
| 5                       | .411740                  | .554300                 | .831211                 | 1.145476                | 1.61031  |
| 6                       | .675727                  | .872085                 | 1.237347                | 1.63539                 | 2.20413  |
| 7                       | .989265                  | 1.239043                | 1.68987                 | 2.16735                 | 2.83311  |
| 8                       | 1.344419                 | 1.646482                | 2.17973                 | 2.73264                 | 3.48954  |
| 9                       | 1.734926                 | 2.087912                | 2.70039                 | 3.32511                 | 4.16816  |
| 10                      | 2.15585                  | 2.55821                 | 3.24697                 | 3.94030                 | 4.86518  |
| 11                      | 2.60321                  | 3.05347                 | 3.81575                 | 4.57481                 | 5.57779  |
| 12                      | 3.07382                  | 3.57056                 | 4.40379                 | 5.22603                 | 6.30380  |
| 13                      | 3.56503                  | 4.10691                 | 5.00874                 | 5.89186                 | 7.04150  |
| 14                      | 4.07468                  | 4.66043                 | 5.62872                 | 6.57063                 | 7.78953  |
| 15                      | 4.60094                  | 5.22935                 | 6.26214                 | 7.26094                 | 8.54675  |
| 16                      | 5.14224                  | 5.81221                 | 6.90766                 | 7.96164                 | 9.31223  |
| 17                      | 5.69724                  | 6.40776                 | 7.56418                 | 8.67176                 | 10.0852  |
| 18                      | 6.26481                  | 7.01491                 | 8.23075                 | 9.39046                 | 10.8649  |
| 19                      | 6.84398                  | 7.63273                 | 8.90655                 | 10.1170                 | 11.6509  |
| 20                      | 7.43386                  | 8.26040                 | 9.59083                 | 10.8508                 | 12.4426  |
| 21                      | 8.03366                  | 8.89720                 | 10.28293                | 11.5913                 | 13.2396  |
| 22                      | 8.64272                  | 9.54249                 | 10.9823                 | 12.3380                 | 14.0415  |
| 23                      | 9.26042                  | 10.19567                | 11.6885                 | 13.0905                 | 14.8479  |
| 24                      | 9.88623                  | 10.8564                 | 12.4011                 | 13.8484                 | 15.6587  |
| 25                      | 10.5197                  | 11.5240                 | 13.1197                 | 14.6114                 | 16.4734  |
| 26                      | 11.1603                  | 12.1981                 | 13.8439                 | 15.3791                 | 17.2919  |
| 27                      | 11.8076                  | 12.8786                 | 14.5733                 | 16.1513                 | 18.1138  |
| 28                      | 12.4613                  | 13.5648                 | 15.3079                 | 16.9279                 | 18.9392  |
| 29                      | 13.1211                  | 14.2565                 | 16.0471                 | 17.7083                 | 19.7677  |
| 30                      | 13.7867                  | 14.9535                 | 16.7908                 | 18.4926                 | 20.5992  |
| 40                      | 20.7065                  | 22.1643                 | 24.4331                 | 26.5093                 | 29.0505  |
| 50                      | 27.9907                  | 29.7067                 | 32.3574                 | 34.7642                 | 37.6886  |
| 60                      | 35.5346                  | 37.4848                 | 40.4817                 | 43.1879                 | 46.4589  |
| 70                      | 43.2752                  | 45.4418                 | 48.7576                 | 51.7393                 | 55.3290  |
| 80                      | 51.1720                  | 53.5400                 | 57.1532                 | 60.3915                 | 64.2778  |
| 90                      | 59.1963                  | 61.7541                 | 65.6466                 | 69.1260                 | 73.2912  |
| 100*                    | 67.3276                  | 70.0648                 | 74.2219                 | 77.9295                 | 82.3581  |

\*For  $df$  greater than 100 the expression  $\sqrt{2\chi^2} - \sqrt{2k-1} = Z$  follows the standardized normal distribution, where  $k$  represents the degrees of freedom





| n   | k' = 11        |                | k' = 12        |                | k' = 13        |                | k' = 14        |                | k' = 15        |                | k' = 16        |                | k' = 17        |                | k' = 18        |                | k' = 19        |                | k' = 20        |                |
|-----|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|
|     | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> |
| 16  | 0.098          | 3.503          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              |
| 17  | 0.138          | 3.378          | 0.087          | 3.557          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              |
| 18  | 0.177          | 3.265          | 0.123          | 3.441          | 0.078          | 3.603          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              |
| 19  | 0.220          | 3.159          | 0.160          | 3.335          | 0.111          | 3.496          | 0.070          | 3.642          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              |
| 20  | 0.263          | 3.063          | 0.200          | 3.234          | 0.145          | 3.395          | 0.100          | 3.542          | 0.063          | 3.676          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              |
| 21  | 0.307          | 2.976          | 0.240          | 3.141          | 0.182          | 3.300          | 0.132          | 3.448          | 0.091          | 3.583          | 0.058          | 3.705          | —              | —              | —              | —              | —              | —              | —              | —              |
| 22  | 0.349          | 2.897          | 0.281          | 3.057          | 0.220          | 3.211          | 0.166          | 3.358          | 0.120          | 3.495          | 0.083          | 3.619          | 0.052          | 3.731          | —              | —              | —              | —              | —              | —              |
| 23  | 0.391          | 2.826          | 0.322          | 2.979          | 0.259          | 3.128          | 0.202          | 3.272          | 0.153          | 3.409          | 0.110          | 3.535          | 0.076          | 3.650          | 0.048          | 3.753          | —              | —              | —              | —              |
| 24  | 0.431          | 2.761          | 0.362          | 2.908          | 0.297          | 3.053          | 0.239          | 3.193          | 0.186          | 3.327          | 0.141          | 3.454          | 0.101          | 3.572          | 0.070          | 3.678          | 0.044          | 3.773          | —              | —              |
| 25  | 0.470          | 2.702          | 0.400          | 2.844          | 0.335          | 2.983          | 0.275          | 3.119          | 0.221          | 3.251          | 0.172          | 3.376          | 0.130          | 3.494          | 0.094          | 3.604          | 0.065          | 3.702          | 0.041          | 3.790          |
| 26  | 0.508          | 2.649          | 0.438          | 2.784          | 0.373          | 2.919          | 0.312          | 3.051          | 0.256          | 3.179          | 0.205          | 3.303          | 0.160          | 3.420          | 0.120          | 3.531          | 0.087          | 3.632          | 0.060          | 3.724          |
| 27  | 0.544          | 2.600          | 0.475          | 2.730          | 0.409          | 2.859          | 0.348          | 2.987          | 0.291          | 3.112          | 0.238          | 3.233          | 0.191          | 3.349          | 0.149          | 3.460          | 0.112          | 3.563          | 0.081          | 3.658          |
| 28  | 0.578          | 2.555          | 0.510          | 2.680          | 0.445          | 2.805          | 0.383          | 2.928          | 0.325          | 3.050          | 0.271          | 3.168          | 0.222          | 3.283          | 0.178          | 3.392          | 0.138          | 3.495          | 0.104          | 3.592          |
| 29  | 0.612          | 2.515          | 0.544          | 2.634          | 0.479          | 2.755          | 0.418          | 2.874          | 0.359          | 2.992          | 0.305          | 3.107          | 0.254          | 3.219          | 0.208          | 3.327          | 0.166          | 3.431          | 0.129          | 3.528          |
| 30  | 0.643          | 2.477          | 0.577          | 2.592          | 0.512          | 2.708          | 0.451          | 2.823          | 0.392          | 2.937          | 0.337          | 3.050          | 0.286          | 3.160          | 0.238          | 3.266          | 0.195          | 3.368          | 0.156          | 3.465          |
| 31  | 0.674          | 2.443          | 0.608          | 2.553          | 0.545          | 2.665          | 0.484          | 2.776          | 0.425          | 2.887          | 0.370          | 2.996          | 0.317          | 3.103          | 0.269          | 3.208          | 0.224          | 3.309          | 0.183          | 3.406          |
| 32  | 0.703          | 2.411          | 0.638          | 2.517          | 0.576          | 2.625          | 0.515          | 2.733          | 0.457          | 2.840          | 0.401          | 2.946          | 0.349          | 3.050          | 0.299          | 3.153          | 0.253          | 3.252          | 0.211          | 3.348          |
| 33  | 0.731          | 2.382          | 0.668          | 2.484          | 0.606          | 2.588          | 0.546          | 2.692          | 0.488          | 2.796          | 0.432          | 2.899          | 0.379          | 3.000          | 0.329          | 3.100          | 0.283          | 3.198          | 0.239          | 3.293          |
| 34  | 0.758          | 2.355          | 0.695          | 2.454          | 0.634          | 2.554          | 0.575          | 2.654          | 0.518          | 2.754          | 0.462          | 2.854          | 0.409          | 2.954          | 0.359          | 3.051          | 0.312          | 3.147          | 0.267          | 3.240          |
| 35  | 0.783          | 2.330          | 0.722          | 2.425          | 0.662          | 2.521          | 0.604          | 2.619          | 0.547          | 2.716          | 0.492          | 2.813          | 0.439          | 2.910          | 0.388          | 3.005          | 0.340          | 3.099          | 0.295          | 3.190          |
| 36  | 0.808          | 2.306          | 0.748          | 2.398          | 0.689          | 2.492          | 0.631          | 2.586          | 0.575          | 2.680          | 0.520          | 2.774          | 0.467          | 2.868          | 0.417          | 2.961          | 0.369          | 3.053          | 0.323          | 3.142          |
| 37  | 0.831          | 2.285          | 0.772          | 2.374          | 0.714          | 2.464          | 0.657          | 2.555          | 0.602          | 2.646          | 0.548          | 2.738          | 0.495          | 2.829          | 0.445          | 2.920          | 0.397          | 3.009          | 0.351          | 3.097          |
| 38  | 0.854          | 2.265          | 0.796          | 2.351          | 0.739          | 2.438          | 0.683          | 2.526          | 0.628          | 2.614          | 0.575          | 2.703          | 0.522          | 2.792          | 0.472          | 2.880          | 0.424          | 2.968          | 0.378          | 3.054          |
| 39  | 0.875          | 2.246          | 0.819          | 2.329          | 0.763          | 2.413          | 0.707          | 2.499          | 0.653          | 2.585          | 0.600          | 2.671          | 0.549          | 2.757          | 0.499          | 2.843          | 0.451          | 2.929          | 0.404          | 3.013          |
| 40  | 0.896          | 2.228          | 0.840          | 2.309          | 0.785          | 2.391          | 0.731          | 2.473          | 0.678          | 2.557          | 0.626          | 2.641          | 0.575          | 2.724          | 0.525          | 2.808          | 0.477          | 2.892          | 0.430          | 2.974          |
| 45  | 0.988          | 2.156          | 0.938          | 2.225          | 0.887          | 2.296          | 0.838          | 2.367          | 0.788          | 2.439          | 0.740          | 2.512          | 0.692          | 2.586          | 0.644          | 2.659          | 0.598          | 2.733          | 0.553          | 2.807          |
| 50  | 1.064          | 2.103          | 1.019          | 2.163          | 0.973          | 2.225          | 0.927          | 2.287          | 0.882          | 2.350          | 0.836          | 2.414          | 0.792          | 2.479          | 0.747          | 2.544          | 0.703          | 2.610          | 0.660          | 2.675          |
| 55  | 1.129          | 2.062          | 1.087          | 2.116          | 1.045          | 2.170          | 1.003          | 2.225          | 0.961          | 2.281          | 0.919          | 2.338          | 0.877          | 2.396          | 0.836          | 2.454          | 0.795          | 2.512          | 0.754          | 2.571          |
| 60  | 1.184          | 2.031          | 1.145          | 2.079          | 1.106          | 2.127          | 1.068          | 2.177          | 1.029          | 2.227          | 0.990          | 2.278          | 0.951          | 2.330          | 0.913          | 2.382          | 0.874          | 2.434          | 0.836          | 2.487          |
| 65  | 1.231          | 2.006          | 1.195          | 2.049          | 1.160          | 2.093          | 1.124          | 2.138          | 1.088          | 2.183          | 1.052          | 2.229          | 1.016          | 2.276          | 0.980          | 2.323          | 0.944          | 2.371          | 0.908          | 2.419          |
| 70  | 1.272          | 1.986          | 1.239          | 2.026          | 1.206          | 2.066          | 1.172          | 2.106          | 1.139          | 2.148          | 1.105          | 2.189          | 1.072          | 2.232          | 1.038          | 2.275          | 1.005          | 2.318          | 0.971          | 2.362          |
| 75  | 1.308          | 1.970          | 1.277          | 2.006          | 1.247          | 2.043          | 1.215          | 2.080          | 1.184          | 2.118          | 1.153          | 2.156          | 1.121          | 2.195          | 1.090          | 2.235          | 1.058          | 2.275          | 1.027          | 2.315          |
| 80  | 1.340          | 1.957          | 1.311          | 1.991          | 1.283          | 2.024          | 1.253          | 2.059          | 1.224          | 2.093          | 1.195          | 2.129          | 1.165          | 2.165          | 1.136          | 2.201          | 1.106          | 2.238          | 1.076          | 2.275          |
| 85  | 1.369          | 1.946          | 1.342          | 1.977          | 1.315          | 2.009          | 1.287          | 2.040          | 1.260          | 2.073          | 1.232          | 2.105          | 1.205          | 2.139          | 1.177          | 2.172          | 1.149          | 2.206          | 1.121          | 2.241          |
| 90  | 1.395          | 1.937          | 1.369          | 1.966          | 1.344          | 1.995          | 1.318          | 2.025          | 1.292          | 2.055          | 1.266          | 2.085          | 1.240          | 2.116          | 1.213          | 2.148          | 1.187          | 2.179          | 1.160          | 2.211          |
| 95  | 1.418          | 1.929          | 1.394          | 1.956          | 1.370          | 1.984          | 1.345          | 2.012          | 1.321          | 2.040          | 1.296          | 2.068          | 1.271          | 2.097          | 1.247          | 2.126          | 1.222          | 2.156          | 1.197          | 2.186          |
| 100 | 1.439          | 1.923          | 1.416          | 1.948          | 1.393          | 1.974          | 1.371          | 2.000          | 1.347          | 2.026          | 1.324          | 2.053          | 1.301          | 2.080          | 1.277          | 2.108          | 1.253          | 2.135          | 1.229          | 2.164          |
| 150 | 1.579          | 1.892          | 1.564          | 1.908          | 1.550          | 1.924          | 1.535          | 1.940          | 1.519          | 1.956          | 1.504          | 1.972          | 1.489          | 1.989          | 1.474          | 2.006          | 1.458          | 2.023          | 1.443          | 2.040          |
| 200 | 1.654          | 1.885          | 1.643          | 1.896          | 1.632          | 1.908          | 1.621          | 1.919          | 1.610          | 1.931          | 1.599          | 1.943          | 1.588          | 1.955          | 1.576          | 1.967          | 1.565          | 1.979          | 1.554          | 1.991          |

Note: n = number of observations, k' = number of explanatory variables excluding the constant term.

Source: This table is an extension of the original Durbin-Watson table and is reproduced from N. E. Savin and K. J. White, "The Durbin-Watson Test for Serial Correlation with Extreme Small Samples or Many Regressors," *Econometrica*, vol. 45, November 1977, pp. 1989-96 and as corrected by R. W. Farebrother, *Econometrica*, vol. 48, September 1980, p. 1554. Reprinted by permission of the Econometric Society.

**EXAMPLE 1**

If  $n = 40$  and  $k' = 4$ ,  $d_L = 1.285$  and  $d_U = 1.721$ . If a computed  $d$  value is less than 1.285, there is evidence of positive first-order serial correlation; if it is greater than 1.721, there is no evidence of positive first-order serial correlation; but if  $d$  lies between the lower and the upper limit, there is inconclusive evidence regarding the presence or absence of positive first-order serial correlation.



| n   | k' = 11        |                | k' = 12        |                | k' = 13        |                | k' = 14        |                | k' = 15        |                | k' = 16        |                | k' = 17        |                | k' = 18        |                | k' = 19        |                | k' = 20        |                |   |
|-----|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|---|
|     | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> | d <sub>L</sub> | d <sub>U</sub> |   |
| 16  | 0.098          | 3.503          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | — |
| 17  | 0.138          | 3.378          | 0.087          | 3.557          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | — |
| 18  | 0.177          | 3.265          | 0.123          | 3.441          | 0.078          | 3.603          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | — |
| 19  | 0.220          | 3.159          | 0.160          | 3.335          | 0.111          | 3.496          | 0.070          | 3.642          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | — |
| 20  | 0.263          | 3.063          | 0.200          | 3.234          | 0.145          | 3.395          | 0.100          | 3.542          | 0.063          | 3.676          | —              | —              | —              | —              | —              | —              | —              | —              | —              | —              | — |
| 21  | 0.307          | 2.976          | 0.240          | 3.141          | 0.182          | 3.300          | 0.132          | 3.448          | 0.091          | 3.583          | 0.058          | 3.705          | —              | —              | —              | —              | —              | —              | —              | —              | — |
| 22  | 0.349          | 2.897          | 0.281          | 3.057          | 0.220          | 3.211          | 0.166          | 3.358          | 0.120          | 3.495          | 0.083          | 3.619          | 0.052          | 3.731          | —              | —              | —              | —              | —              | —              | — |
| 23  | 0.391          | 2.826          | 0.322          | 2.979          | 0.259          | 3.128          | 0.202          | 3.272          | 0.153          | 3.409          | 0.110          | 3.535          | 0.076          | 3.650          | 0.048          | 3.753          | —              | —              | —              | —              | — |
| 24  | 0.431          | 2.761          | 0.362          | 2.908          | 0.297          | 3.053          | 0.239          | 3.193          | 0.186          | 3.327          | 0.141          | 3.454          | 0.101          | 3.572          | 0.070          | 3.678          | 0.044          | 3.773          | —              | —              | — |
| 25  | 0.470          | 2.702          | 0.400          | 2.844          | 0.335          | 2.983          | 0.275          | 3.119          | 0.221          | 3.251          | 0.172          | 3.376          | 0.130          | 3.494          | 0.094          | 3.604          | 0.065          | 3.702          | 0.041          | 3.790          | — |
| 26  | 0.508          | 2.649          | 0.438          | 2.784          | 0.373          | 2.919          | 0.312          | 3.051          | 0.256          | 3.179          | 0.205          | 3.303          | 0.160          | 3.420          | 0.120          | 3.531          | 0.087          | 3.632          | 0.060          | 3.724          | — |
| 27  | 0.544          | 2.600          | 0.475          | 2.730          | 0.409          | 2.859          | 0.348          | 2.987          | 0.291          | 3.112          | 0.238          | 3.233          | 0.191          | 3.349          | 0.149          | 3.460          | 0.112          | 3.563          | 0.081          | 3.658          | — |
| 28  | 0.578          | 2.555          | 0.510          | 2.680          | 0.445          | 2.805          | 0.383          | 2.928          | 0.325          | 3.050          | 0.271          | 3.168          | 0.222          | 3.283          | 0.178          | 3.392          | 0.138          | 3.495          | 0.104          | 3.592          | — |
| 29  | 0.612          | 2.515          | 0.544          | 2.634          | 0.479          | 2.755          | 0.418          | 2.874          | 0.359          | 2.992          | 0.305          | 3.107          | 0.254          | 3.219          | 0.208          | 3.327          | 0.166          | 3.431          | 0.129          | 3.528          | — |
| 30  | 0.643          | 2.477          | 0.577          | 2.592          | 0.512          | 2.708          | 0.451          | 2.823          | 0.392          | 2.937          | 0.337          | 3.050          | 0.286          | 3.160          | 0.238          | 3.266          | 0.195          | 3.368          | 0.156          | 3.465          | — |
| 31  | 0.674          | 2.443          | 0.608          | 2.553          | 0.545          | 2.665          | 0.484          | 2.776          | 0.425          | 2.887          | 0.370          | 2.996          | 0.317          | 3.103          | 0.269          | 3.208          | 0.224          | 3.309          | 0.183          | 3.406          | — |
| 32  | 0.703          | 2.411          | 0.638          | 2.517          | 0.576          | 2.625          | 0.515          | 2.733          | 0.457          | 2.840          | 0.401          | 2.946          | 0.349          | 3.050          | 0.299          | 3.153          | 0.253          | 3.252          | 0.211          | 3.348          | — |
| 33  | 0.731          | 2.382          | 0.668          | 2.484          | 0.606          | 2.588          | 0.546          | 2.692          | 0.488          | 2.796          | 0.432          | 2.899          | 0.379          | 3.000          | 0.329          | 3.100          | 0.283          | 3.198          | 0.239          | 3.293          | — |
| 34  | 0.758          | 2.355          | 0.695          | 2.454          | 0.634          | 2.554          | 0.575          | 2.654          | 0.518          | 2.754          | 0.462          | 2.854          | 0.409          | 2.954          | 0.359          | 3.051          | 0.312          | 3.147          | 0.267          | 3.240          | — |
| 35  | 0.783          | 2.330          | 0.722          | 2.425          | 0.662          | 2.521          | 0.604          | 2.619          | 0.547          | 2.716          | 0.492          | 2.813          | 0.439          | 2.910          | 0.388          | 3.005          | 0.340          | 3.099          | 0.295          | 3.190          | — |
| 36  | 0.808          | 2.306          | 0.748          | 2.398          | 0.689          | 2.492          | 0.631          | 2.586          | 0.575          | 2.680          | 0.520          | 2.774          | 0.467          | 2.868          | 0.417          | 2.961          | 0.369          | 3.053          | 0.323          | 3.142          | — |
| 37  | 0.831          | 2.285          | 0.772          | 2.374          | 0.714          | 2.464          | 0.657          | 2.555          | 0.602          | 2.646          | 0.548          | 2.738          | 0.495          | 2.829          | 0.445          | 2.920          | 0.397          | 3.009          | 0.351          | 3.097          | — |
| 38  | 0.854          | 2.265          | 0.796          | 2.351          | 0.739          | 2.438          | 0.683          | 2.526          | 0.628          | 2.614          | 0.575          | 2.703          | 0.522          | 2.792          | 0.472          | 2.880          | 0.424          | 2.968          | 0.378          | 3.054          | — |
| 39  | 0.875          | 2.246          | 0.819          | 2.329          | 0.763          | 2.413          | 0.707          | 2.499          | 0.653          | 2.585          | 0.600          | 2.671          | 0.549          | 2.757          | 0.499          | 2.843          | 0.451          | 2.929          | 0.404          | 3.013          | — |
| 40  | 0.896          | 2.228          | 0.840          | 2.309          | 0.785          | 2.391          | 0.731          | 2.473          | 0.678          | 2.557          | 0.626          | 2.641          | 0.575          | 2.724          | 0.525          | 2.808          | 0.477          | 2.892          | 0.430          | 2.974          | — |
| 45  | 0.988          | 2.156          | 0.938          | 2.225          | 0.887          | 2.296          | 0.838          | 2.367          | 0.788          | 2.439          | 0.740          | 2.512          | 0.692          | 2.586          | 0.644          | 2.659          | 0.598          | 2.733          | 0.553          | 2.807          | — |
| 50  | 1.064          | 2.103          | 1.019          | 2.163          | 0.973          | 2.225          | 0.927          | 2.287          | 0.882          | 2.350          | 0.836          | 2.414          | 0.792          | 2.479          | 0.747          | 2.544          | 0.703          | 2.610          | 0.660          | 2.675          | — |
| 55  | 1.129          | 2.062          | 1.087          | 2.116          | 1.045          | 2.170          | 1.003          | 2.225          | 0.961          | 2.281          | 0.919          | 2.338          | 0.877          | 2.396          | 0.836          | 2.454          | 0.795          | 2.512          | 0.754          | 2.571          | — |
| 60  | 1.184          | 2.031          | 1.145          | 2.079          | 1.106          | 2.127          | 1.068          | 2.177          | 1.029          | 2.227          | 0.990          | 2.278          | 0.951          | 2.330          | 0.913          | 2.382          | 0.874          | 2.434          | 0.836          | 2.487          | — |
| 65  | 1.231          | 2.006          | 1.195          | 2.049          | 1.160          | 2.093          | 1.124          | 2.138          | 1.088          | 2.183          | 1.052          | 2.229          | 1.016          | 2.276          | 0.980          | 2.323          | 0.944          | 2.371          | 0.908          | 2.419          | — |
| 70  | 1.272          | 1.986          | 1.239          | 2.026          | 1.206          | 2.066          | 1.172          | 2.106          | 1.139          | 2.148          | 1.105          | 2.189          | 1.072          | 2.232          | 1.038          | 2.275          | 1.005          | 2.318          | 0.971          | 2.362          | — |
| 75  | 1.308          | 1.970          | 1.277          | 2.006          | 1.247          | 2.043          | 1.215          | 2.080          | 1.184          | 2.118          | 1.153          | 2.156          | 1.121          | 2.195          | 1.090          | 2.235          | 1.058          | 2.275          | 1.027          | 2.315          | — |
| 80  | 1.340          | 1.957          | 1.311          | 1.991          | 1.283          | 2.024          | 1.253          | 2.059          | 1.224          | 2.093          | 1.195          | 2.129          | 1.165          | 2.165          | 1.136          | 2.201          | 1.106          | 2.238          | 1.076          | 2.275          | — |
| 85  | 1.369          | 1.946          | 1.342          | 1.977          | 1.315          | 2.009          | 1.287          | 2.040          | 1.260          | 2.073          | 1.232          | 2.105          | 1.205          | 2.139          | 1.177          | 2.172          | 1.149          | 2.206          | 1.121          | 2.241          | — |
| 90  | 1.395          | 1.937          | 1.369          | 1.966          | 1.344          | 1.995          | 1.318          | 2.025          | 1.292          | 2.055          | 1.266          | 2.085          | 1.240          | 2.116          | 1.213          | 2.148          | 1.187          | 2.179          | 1.160          | 2.211          | — |
| 95  | 1.418          | 1.929          | 1.394          | 1.956          | 1.370          | 1.984          | 1.345          | 2.012          | 1.321          | 2.040          | 1.296          | 2.068          | 1.271          | 2.097          | 1.247          | 2.126          | 1.222          | 2.156          | 1.197          | 2.186          | — |
| 100 | 1.439          | 1.923          | 1.416          | 1.948          | 1.393          | 1.974          | 1.371          | 2.000          | 1.347          | 2.026          | 1.324          | 2.053          | 1.301          | 2.080          | 1.277          | 2.108          | 1.253          | 2.135          | 1.229          | 2.164          | — |
| 150 | 1.579          | 1.892          | 1.564          | 1.908          | 1.550          | 1.924          | 1.535          | 1.940          | 1.519          | 1.956          | 1.504          | 1.972          | 1.489          | 1.989          | 1.474          | 2.006          | 1.458          | 2.023          | 1.443          | 2.040          | — |
| 200 | 1.654          | 1.885          | 1.643          | 1.896          | 1.632          | 1.908          | 1.621          | 1.919          | 1.610          | 1.931          | 1.599          | 1.943          | 1.588          | 1.955          | 1.576          | 1.967          | 1.565          | 1.979          | 1.554          | 1.991          | — |

Note: n = number of observations, k' = number of explanatory variables excluding the constant term

Source: This table is an extension of the original Durbin-Watson table and is reproduced from N. E. Savin and K. J. White, "The Durbin-Watson Test for Serial Correlation with Extreme Small Samples or Many Regressors," *Econometrica*, vol. 45, November 1977, pp. 1989-96 and as corrected by R. W. Farebrother, *Econometrica*, vol. 48, September 1980, p. 1554. Reprinted by permission of the Econometric Society.

**EXAMPLE 1**

If  $n = 40$  and  $k' = 4$ ,  $d_L = 1.285$  and  $d_U = 1.721$ . If a computed  $d$  value is less than 1.285, there is evidence of positive first-order serial correlation; if it is greater than 1.721, there is no evidence of positive first-order serial correlation; but if  $d$  lies between the lower and the upper limit, there is inconclusive evidence regarding the presence or absence of positive first-order serial correlation.



Stockholms  
universitet

Statistiska institutionen

## Rättningsblad

**Datum:** 27/4-2017

**Sal:** Brunnsvikssalen

**Tenta:** Regressionsanalys

**Kurs:** Ekonometri

**ANONYMKOD:**

EKR-0014



Jag godkänner att min tenta får läggas ut anonymt på hemsidan som studentsvar.

**OBS! SKRIV ÄVEN PÅ BAKSIDAN AV SKRIVBLADEN**

Markera besvarade uppgifter med kryss

| 1               | 2  | 3  | 4  | 5  | 6 | 7 | 8 | 9 | Antal inl. blad |
|-----------------|----|----|----|----|---|---|---|---|-----------------|
| X               | X  | X  | X  | X  |   |   |   |   | 5 Bl            |
| Lär. ant.<br>22 | 25 | 17 | 12 | 15 |   |   |   |   |                 |

|       |    |       |   |                |     |
|-------|----|-------|---|----------------|-----|
| POÄNG | 94 | BETYG | A | Lärarens sign. | PKA |
|-------|----|-------|---|----------------|-----|

Exercise 1

- $y$  - life time (in min.) of a cutting tool.
- $X$  - speed (rounds/minute); A, B - types of tools.
- $G_i = \beta_0 + \beta_1 X_i + \beta_2 D_i + \epsilon_i$ ,  $n = 20$

$$D = \begin{cases} 1 & \text{if B} \\ 0 & \text{if A} \end{cases}$$

$$a) R^2 = \frac{ESS}{TSS} = \frac{1418,034}{1545,089} \approx 0,90 \approx (90\%)$$

$$\begin{aligned} \bar{R}^2 &= 1 - \frac{RSS/(n-k)}{TSS/(n-1)} = 1 - \frac{154,055/17}{1545,089/19} \\ &= 1 - \frac{9,2385}{82,8994} \approx 1 - 0,1114 \approx 0,889 \approx 88,9\% \end{aligned}$$

Answer:  $R^2 \approx 90\%$ ,  $\bar{R}^2 \approx 88,9\%$

OK

b) We test this with a general F-test.

• Hypotheses:

$$H_0: \beta_2 = \beta_3 = 0$$

$H_a$ : at least one of the  $\beta_i$ 's is  $\neq 0$ .

• Test statistics:  $F = \frac{ESS/(k-1)}{RSS/(n-k)}$

$F(k-1, n-k; \alpha)$

• Fcrit  $(2, 17) = 6,11$

• Decision: if  $F_{obs} > F_{crit}$  we reject  $H_0$  in favor of  $H_a$

•  $F_{obs}$   $= \frac{1418,034/2}{154,055/17} = \frac{709,017}{9,2385} \approx 76,7$

Ex 1. cont

Answer:  $F_{obs} = 46,7 > F_{crit} = 6,14$ , therefore we reject  $H_0$  at 10% sign level. We've got evidence that at least one of the expl. variables should be in the model. OK

d) The model  $y_i = \beta_1 + \beta_2 \cdot X_i + \beta_3 \cdot D_i + u_i$ .  
Our model includes the intercept term and a dummy variable. It means that we treat  $\beta_1$  not only as intercept, but also as the reference base (at least theoretically). Therefore  $\beta_1$  represents here the (average) effective life time of a type A tool. Then  $\beta_3$  is a differential effect for a type B tool (compared with a type A).

$$\hat{y}_i = 36,986 - 0,024 \cdot X_i + 15,004 \cdot D_i$$

$\rightarrow \beta_1 =$  (average) effective life time of a type A tool. = 36,986

$\rightarrow \beta_3 =$  indicates that the (average) effective life time of a type B tool differs from that of a type A by +15,004 and is equal to  $36,986 + 15,004 = 51,99$ , holding  $X$  constant (essentially when  $X = 0$ ).

Answer: The expectation life time of a type B tool is 51,99 (mins).

Cont. Ex. 1

d) C.I. for  $\beta_3$  at 95%:

$$\bar{\beta}_3 \pm t_{\alpha/2}^{(n-k)} \cdot SE(\bar{\beta}_3)$$

•  $\bar{\beta}_3 = 15,004$

•  $SE(\bar{\beta}_3) = 1,36 \Rightarrow 15,004 \pm 2,11 \cdot 1,36 =$

•  $t_{0,025}^{(14)} = 2,11 \Rightarrow = 15,004 \pm 2,8696$

Answer  $\bar{I}_{\beta_3}^{\alpha=0,05} = [12,13; 17,87]$  OK

e) (1):  $y_i = \beta_1 + \beta_2 \cdot X_i + \beta_3 \cdot D_i + u_i$

(2):  $y_i = \beta_1 + \beta_2 \cdot X_i + \beta_3 \cdot D_i + \beta_4 \cdot X_i \cdot D_i + u_i$

The effective (expected) life time ( $y$ ) depends on (if  $D = 1$ , type B tool).

→ In model (1):  $\hat{y} = \hat{\beta}_1 + \hat{\beta}_2 \cdot X_i + \hat{\beta}_3 = (\hat{\beta}_1 + \hat{\beta}_3) + \hat{\beta}_2 \cdot X_i \rightarrow$  it will be determined by the speed, ~~whether~~ it is the speed of a type A or a type B tool is unspecified.

→ In model (2):  $\hat{y} = \hat{\beta}_1 + \hat{\beta}_2 \cdot X_i + \hat{\beta}_3 + \hat{\beta}_4 \cdot X_i = (\hat{\beta}_1 + \hat{\beta}_3) + (\hat{\beta}_2 + \hat{\beta}_4) \cdot X_i$

here, the expected effective life time  $y$  for a type B tool will be influenced by the speed of a type B tool and will be "corrected" by  $\hat{\beta}_4$  (differential effect of the speed of a type B tool). In this respect the model (2) is richer OK

Ex cont.

1) Test stat:  $F = \frac{(R_{\text{old}} - R_{\text{new}}) / \text{number of } x_i \text{ in } H_0}{(1 - R_{\text{new}}) / (n - k) \text{ number of } x_i \text{ in } H_1 \text{ new model}}$

Let  $F(m; n-k)$

$H_0$ : the term  $x_i \cdot D_i$  does not contribute significantly to the model

$H_{a1}$ : it does contribute significantly to the model

Note: we can use  $k^2$  in the test as both  $H_0$  and  $H_1$  in two model have the same form (function).

$F_{\text{crit}}(10, 05) = 4,49$   
(critical)

Decision: if  $F_{\text{obs}} > F_{\text{crit}} \rightarrow$  reject  $H_0$ .

$R_{\text{new}} = \frac{ESS_{\text{new}}}{TSS} = \frac{1434,112}{1575,089} \approx 0,91$

$F_{\text{obs}} = \frac{(0,91 - 0,90) / 1}{(1 - 0,91) / 16} = \frac{0,01}{0,005625} \approx 1,78$

Answer: as  $F_{\text{obs}} \approx 1,78 < F_{\text{crit}} = 4,49$  we can not reject the  $H_0$  and therefore we can not conclude that the new model is better (we did not get enough evidence that  $x_i \cdot D_i$  should be included) at  $\alpha = 0,05$ .

OK

Exercise 2

$Q = \beta_1 \cdot L^{\beta_2} \cdot K^{\beta_3}$ ,  $L =$  labor input,  $K =$  cap stock  
 $y = \ln(Q)$  as dependent in a linear R.M.

a)  $\ln(Q) = \ln \beta_1 + \beta_2 \cdot \ln(L) + \beta_3 \cdot \ln(K) + u_i$

OK

Op. 2, cont.

b)  $\beta_3 = 1 - \beta_2$

$$\begin{aligned} \ln(Q) &= \ln \beta_1 + \beta_2 \ln(L) + (1 - \beta_2) \cdot \ln K + u_i \\ &= \ln \beta_1 + \beta_2 \ln(L) + \ln K - \beta_2 \cdot \ln K + u_i \\ &= \ln \beta_1 + \ln K + \beta_2 (\ln(L) - \ln(K)) + u_i \end{aligned}$$

$$\ln(Q) - \ln(K) = \ln \beta_1 + \beta_2 (\ln(L) - \ln(K)) + u_i$$

$$\begin{aligned} \Rightarrow \ln\left(\frac{Q}{K}\right) &= \ln \beta_1 + \beta_2 \ln\left(\frac{L}{K}\right) + u_i \\ &= \beta_1' + \beta_2 \cdot \ln\left(\frac{L}{K}\right) + u_i \\ \text{where } \beta_1' &= \ln \beta_1 \end{aligned}$$

OK

c)  $n = 33$

(1)  $\ln Q = \ln \beta_1 + \beta_2 \cdot \ln L + \beta_3 \cdot \ln K + u_i$

(2)  $\ln\left(\frac{Q}{K}\right) = \ln \beta_1 + \beta_2 \cdot \ln\left(\frac{L}{K}\right) + u_i$

Since we have used 1 restriction, namely  $\beta_3 = 1 - \beta_2$ , to obtain the model (2), I suggest to use F-restricted or a test statistics at  $\alpha = 0,05$ .

$H_0$ : The restricted model (2) is better

$H_1$ : The unrestricted model (1) is better

• Test stat:  $F = \frac{(ESSR - RSS_{ur})/m}{RSS_{ur}/(n-k)}$   $\stackrel{H_0}{\sim} F(1, 30)$

•  $F_{crit}(1, 30) = 1,7$

OK

## Exp. 2, cont

• reject  $H_0$  if  $F_{obs} > F_{crit} = 4,17$  at  $\alpha = 0,05$ .

d) One potential advantage, from a modelling point of view, is that model  $\ln(Q)$  is built on ratios  $\frac{Q}{K}$  and  $\frac{L}{K}$ , which are used in economics and designate  $\frac{L}{K}$  = labour/capital ratio, and

$\frac{Q}{K}$  = production/capital ratio. From

this model we can directly estimate the elasticity of  $\frac{Q}{K}$  with respect to a unit (10%) change in  $\frac{L}{K}$ . OK

$$e) \ln Q = \ln \beta_0 + \beta_1 \cdot \ln\left(\frac{L}{K}\right) + \beta_2 \cdot \ln\left(\frac{Q}{K}\right) + \epsilon$$

$$\cdot \hat{\rho} = 0,6, \alpha = 0,05$$

$$\cdot 1890 - 1922, n = 24$$

→ In order to draw the conclusion about the presence of positive autocorrelation we have to find out the Durbin Watson d statistic. We can do it on the basis of  $\hat{\rho}$ , knowing that:

$$d \approx 2(1 - \hat{\rho}) \approx 2(1 - 0,6) = 0,8$$

→ Critical values for d at  $\alpha = 0,05$  ( $\frac{n}{N} = \frac{24}{24}$ )

$$d_L = 1,188$$

$$d_U = 1,546$$

→  $d = 0,8 < d_L = 1,188$ , which does confirm that we have evidence of a positive autocorrelation. OK



Exercise 3

- $n = 108$  (single households),  
 $y = \text{rent}$ ,  $x = \text{income}$
- $y = \beta_1 + \beta_2 \cdot x + u_i$  (simple linear).

$$a) u_i^2 = \beta_1 + \beta_2 \cdot x + \beta_3 \cdot x^2 + v_i$$

$$b) n = 108, R_{(max)}^2 = 0,082134.$$

- Test statistic:  $n \cdot R^2 \stackrel{H_0}{\sim} \chi^2(2)$

- $n \cdot R^2 = 108 \cdot 0,082134 \approx 8,87$

- $\chi_{obs}^2(2) = 5,99$

Answer:  $\chi_{obs}^2 = 8,87 > \chi_{crit}^2 = 5,99$ , therefore we can reject  $H_0$  at 5% sign level. We've got evidence of heteroskedasticity in the model.

$$c) V(u_i) = z^2 \cdot x_i$$

Mathematically:

$$V(a \cdot u_i) = a^2 \cdot V(u_i) = a^2 \cdot z^2 \cdot x_i$$

We seek:  $a^2 \cdot z^2 \cdot x_i = z^2$

$$a^2 = \frac{1}{x_i} \rightarrow a = \frac{1}{\sqrt{x_i}}$$

Why to correct for the heteroskedasticity in our model we can transform our data by dividing it by  $\sqrt{x_i}$ :

$$\frac{y_i}{\sqrt{x_i}} = \frac{\beta_1}{\sqrt{x_i}} + \frac{\beta_2 \cdot x_i}{\sqrt{x_i}} + \frac{u_i}{\sqrt{x_i}} = \frac{\beta_1}{\sqrt{x_i}} + \beta_2 \sqrt{x_i} + \frac{u_i}{\sqrt{x_i}}$$

("no-intercept" model).

## Exercise 4

- a) True model:  $y_i = \beta_1 + \beta_2 x_i + u_i$   
 Using:  $(y_i - c_1) = \beta_1 + \beta_2 (x_i - c_2) + u_i$

d) We are using the formulas:

$$\hat{\beta}_1 = \bar{y} - \hat{\beta}_2 \bar{x}$$

$$\hat{\beta}_2 = \frac{\sum (x_i - \bar{x})(y_i - \bar{y})}{\sum (x_i - \bar{x})^2}$$

$c_1$  and  $c_2$  are known constants!

$(y_i - c_1) = \beta_1 + \beta_2 (x_i - c_2) + u_i$

$y^* = \beta_1 + \beta_2 x^* + u_i$

We use the fact that

$\bar{x}^* = \overline{x_i - c_2} = \bar{x} - c_2$ , ( $c_2$  is a constant),

$\bar{y}^* = \overline{y_i - c_1} = \bar{y} - c_1$

$\hat{\beta}_2 = \frac{\sum (x_i^* - \bar{x}^*)(y_i^* - \bar{y}^*)}{\sum (x_i^* - \bar{x}^*)^2} = \frac{\sum (x_i - c_2 - (\bar{x} - c_2))(y_i - c_1 - (\bar{y} - c_1))}{\sum (x_i - c_2 - (\bar{x} - c_2))^2}$

$= \frac{\sum (x_i - \bar{x})(y_i - \bar{y})}{\sum (x_i - \bar{x})^2} = \hat{\beta}_2$  OLS estimator for  $\hat{\beta}_2$  OK

$\hat{\beta}_1 = \bar{y}^* - \hat{\beta}_2 \bar{x}^* = \bar{y} - c_1 - \hat{\beta}_2 (\bar{x} - c_2) = \bar{y} - \hat{\beta}_2 (\bar{x} - c_2) - c_1$  OLS estimator for  $\hat{\beta}_1$  OK

- b)  $E(\hat{\beta}_2) = \beta_2$  - an unbiased estimator,  
 $E(\hat{\beta}_1) \neq \beta_1$  - biased, basically it is derived from  $y_i = (\beta_1 + c) + \beta_2 (x_i - c) + u_i$  + continued on the last page

Exercise 5

a) If  $X$  is divided by 2, then:

$$\hat{\beta}_2^* = \frac{\sum \left( \frac{X_i}{2} - \frac{\bar{X}}{2} \right) (Y_i - \bar{Y})}{\sum \left( \frac{X_i}{2} - \frac{\bar{X}}{2} \right)^2} =$$

$$= \frac{\frac{1}{2} \sum (X_i - \bar{X}) (Y_i - \bar{Y})}{\frac{1}{4} \sum (X_i - \bar{X})^2} = 2 \cdot \hat{\beta}_2$$

$$\hat{\beta}_1^* = \bar{Y} - \hat{\beta}_2^* \cdot \frac{\bar{X}}{2} = \bar{Y} - 2 \hat{\beta}_2 \cdot \frac{\bar{X}}{2} = \bar{Y} - \hat{\beta}_2 \cdot \bar{X} = \hat{\beta}_1$$

FALSE. Only  $\hat{\beta}_1$  is unchanged

OK

b)  $Y_i = \beta_1 + \beta_2 X_i + u_i$ ,  $Y_i^* = Y_i + \epsilon_i$  /  $\epsilon_i$  is uncorrelated w/  $Y_i^*$  (and  $Y_i$ ),  $E(\epsilon_i) = 0$  (usual assumption)

$$Y_i^* - \epsilon_i = \beta_1 + \beta_2 X_i + u_i$$

$$Y_i^* = \beta_1 + \beta_2 X_i + (u_i + \epsilon_i)$$

$$\Rightarrow \text{Cov}(X_i, u_i) = 0, \text{Cov}(u_i + \epsilon_i) = 0.$$

FALSE.  $X$  and error term are uncorrelated

OK

c) FALSE. The test is used to check if there is autocorrelation. So, if the disturbance variables are autocorrelated, it is used to detect it. One remark here

OK

It is used a way to detect multicollinearity in the presence of the first-order Markov correlated error scheme, i.e., (AR1):  $u_t = \rho \cdot u_{t-1} + \epsilon_t$ .

d) FALSE. COVARIANCE can be any number, it is coefficient of correlation  $\rho(\beta)$  that lies in the interval  $[-1, 1]$ , which is determined (if I remember it correctly) as  $\rho = \frac{\text{cov}(X, Y)}{SE_X \cdot SE_Y}$ . OK

e) TRUE ~~FALSE~~ It can be one of the reasons of heteroskedasticity (i.e.  $V(u_i) = \sigma^2 X_i$ , though it's not the only reason. OK

f) FALSE ✓ The runs test doesn't rely on the assumption of normality. It's the Durbin Watson & test (modified test to detect autocorrelation) that relies on it. 1/3

\* Exercise 4, cont.

$$\begin{aligned} E(\hat{\beta}_1) &= E(\bar{y} - \beta_0 \bar{x} + \hat{\beta}_2 (c_2 - c_1)) = \\ &= E(\bar{y} - \beta_0 \bar{x}) + E(\hat{\beta}_2 (c_2 - c_1)) = \\ &= E(\hat{\beta}_1) + E(\hat{\beta}_2 (c_2 - c_1)) - E(c_1) = \\ &= \beta_1 + \underbrace{c_2 \cdot \beta_2 - c_1}_{\text{bias}} \end{aligned}$$

$E(\hat{\beta}_1) \neq \beta_1$  OK 1/3



Stockholms  
universitet

Statistiska institutionen

## Rättningsblad

**Datum:** 27/4-2017

**Sal:** ~~Brunnsvikssalen~~ UG

**Tenta:** Regressionsanalys

**Kurs:** Ekonometri

**ANONYMKOD:**

EKR-0025

Jag godkänner att min tenta får läggas ut anonymt på hemsidan som studentsvar.

**OBS! SKRIV ÄVEN PÅ BAKSIDAN AV SKRIVBLADEN**

Markera besvarade uppgifter med kryss

| 1              | 2  | 3  | 4  | 5  | 6 | 7 | 8 | 9 | Antal inl. blad |
|----------------|----|----|----|----|---|---|---|---|-----------------|
| X              | X  | X  | X  | X  |   |   |   |   | 6 82            |
| Lär.ant.<br>23 | 20 | 20 | 15 | 16 |   |   |   |   |                 |

|       |    |       |   |                |      |
|-------|----|-------|---|----------------|------|
| POÄNG | 89 | BETYG | A | Lärarens sign. | Pget |
|-------|----|-------|---|----------------|------|

$$1) \quad Y_i = \beta_1 + \beta_2 X_i + \beta_3 D_i + u_i \quad n=20$$

$$k=3$$

a) (coeff. of determination)  $R^2 = 1 - \frac{RSS}{TSS} = 1 - \frac{157,055}{1575,089} = 0,900$

Adjusted  $\bar{R}^2 = 1 - \frac{RSS / (n-k)}{TSS / (n-1)} = 1 - \frac{157,055 / (20-3)}{1575,089 / (20-1)}$

$$ESS = 1418,034$$

$$RSS = 157,055$$

$$TSS = 1575,089$$

$$= 0,889$$

$$R^2 = 0,900 \quad \bar{R}^2 = 0,889 \quad \text{OK}$$

b)  $H_0: \beta_2 = \beta_3 = 0$  (none of the variables influence  $Y$ )

$H_A$ : At least one of  $\beta_2$  or  $\beta_3$  is not 0

General F-test for  $H_0$ :  $F = \frac{ESS / (k-1)}{RSS / (n-k)} = \frac{1418,034 / 2}{157,055 / 17}$

$$\Rightarrow F = 76,7416$$

Critical F from table

$$F_{0,01}(2, 17) = 6,11$$

$$F > F_{crit}$$

$\Rightarrow H_0$  is rejected and at least one of  $\beta_2$  or  $\beta_3$  should be included in the model

OK

$$\text{Type A } E(Y_i | D=0) = \beta_1 + \beta_2 X_i$$

$$\text{Type B } E(Y_i | D=1) = \beta_1 + \beta_2 X_i + \beta_3$$

$\beta_3$  is the difference in the expected value of  $Y$  for a given  $X$  i.e. the difference in lifetime between A and B for a given speed.

d) 95% confidence interval

$$\frac{\hat{\beta}_i - \beta_i}{\text{se}(\hat{\beta}_i)} \sim t(n-k)$$

Under  $H_0: \beta_i = 0$

$$\hat{\beta}_i \pm t(n-k) \cdot \text{se}(\hat{\beta}_i)$$

$$\hat{\beta}_3 \pm t_{0,05}(17) \cdot \text{se}(\hat{\beta}_3)$$

$$15,004 \pm \underbrace{2,11 \cdot 1,36}_{2,8696}$$

$$12,13 - 17,87$$

95% conf. interval for  $\beta_3$

OK

Uppgift 1  
e)

$$Y_i = \beta_1 + \beta_2 X_i + \beta_3 D_i + \beta_4 X_i D_i + u_i$$

This model also includes an interaction term between  $X_i$  and  $D_i$ , the speed and the type. Therefore this model can account for a possible interaction between speed and type that is multiplicative?,  $\beta_4 X_i D_i$ .

 $k=4$   
 $n=20$ 

f) Test if the new model is sign. better.

 $H_0$ : The new model is not sign. better than the old.

 $H_A$ : The new -||- is better.

$$F = \frac{(ESS_{\text{new}} - ESS_{\text{old}}) / 1}{RSS_{\text{new}} / (n - 4)} = \frac{1434,112 - 1418,034}{140,977 / 16}$$

$$ESS_{\text{new}} = 1434,112$$

$$ESS_{\text{old}} = 1418,034$$

$$RSS_{\text{new}} = 140,977$$

$$\Rightarrow F = 1,82$$

$$F_{0,05}(1,16) = 4,49 \text{ (table)}$$

$F < F_{\text{crit}}$  so  $H_0$  is not rejected and the interaction term should not be included in the model

OK / 23



Uppgift 2

$$Q = \beta_1 L^{\beta_2} K^{\beta_3}$$

L = labour input

K = capital stock

$$a) Y = \ln Q = \underbrace{\ln \beta_1}_{\alpha_1} + \beta_2 \ln L + \beta_3 \ln K + u_i$$

$$b) \beta_3 = 1 - \beta_2 \Rightarrow Y = \alpha_1 + \beta_2 \ln L + (1 - \beta_2) \ln K + u_i$$

$$\Rightarrow Y = \alpha_1 + \beta_2 (\ln L - \ln K) + \ln K + u_i$$

$$Y - \ln K = \alpha_1 + \beta_2 (\ln L - \ln K) + u_i$$

c) To test the assumption that  $\beta_2 = 1 - \beta_3$   
we set up

$$H_0: \beta_2 + \beta_3 = 1$$

$$H_A: \beta_2 + \beta_3 \neq 1$$

$$\frac{\hat{\beta}_i - \beta_i}{\text{se}(\hat{\beta}_i)} \sim t(n-k)$$

$$\text{Under } H_0 \quad \frac{\hat{\beta}_2 + \hat{\beta}_3 - 1}{\text{se}(\hat{\beta}_2 + \hat{\beta}_3)} \sim t(33 - 3 = 30)$$

Inte sant all  
 $E(\hat{\beta}_2 + \hat{\beta}_3) = 1$   
 under  $H_0$ .

If  $t < -2,042$  or  $t > 2,042$   
 we reject  $H_0$  and do not  
 implement  $\beta_2 + \beta_3 = 1$  in the  
 model

d) If  $\beta_3 = 1 - \beta_2$  and we have both  $\beta_2$  and  $\beta_3$  in the model as we have in a) we will have a problem with collinearity as  $\beta_3$  is a linear function of  $\beta_2$ . Model b) might solve this problem. <sup>might</sup>

e) I don't remember how to calculate  $d$  from  $\hat{\rho}$  but if I could calculate  $d$  I would compare to  $d_L$  in Durbin Watson table  $k' = 2$   $n = 24$  (1899-1922 yearly)

Change to 5% significance as table is missing

$$d_L = 1,188 \quad d_U = 1,546$$

If  $d \leq d_L$  there is positive auto correlation

~~PPA~~

1/20

Uppgift 3.

~~Y~~  
~~Y~~  
~~Y~~

$$Y = \beta_1 + \beta_2 X + u_i$$

Y: Rent  
X: Income

a) White's auxiliary regression

$$\hat{u}_i^2 = \alpha_1 + \alpha_2 X + \alpha_3 X^2 + \varepsilon_i$$

OK

b)  $H_0$ : Homoscedasticity  $\alpha_2 = \alpha_3 = 0$  $H_A$ : Heteroscedasticity

$$n R^2 \sim \chi^2(2) \quad \text{approx. under } H_0$$

$$n = 108 \quad R^2 = 0,082134 \Rightarrow n \cdot R^2 = 8,87$$

$$\chi_{0,05}^2(2) = 5,991$$

$$\text{Calculated } \chi^2 = n R^2 > \chi_{0,05}^2(2)$$

 $H_0$  is rejectedThere is  
heteroscedasticity

OK

3.c

$$V(u_i) = \sigma^2 X_i$$

$$Y = \beta_1 + \beta_2 X_i + u_i$$

$$V\left(\frac{u_i}{\sqrt{X_i}}\right) = \frac{1}{X_i} \cdot V(u_i) = \frac{1}{X_i} \cdot \sigma^2 X_i = \sigma^2$$

homoscedasticity

$X_i$  is not random

The model can be transformed to obtain homosced.

$$\frac{Y_i}{\sqrt{X_i}} = \beta_1 \cdot \frac{1}{\sqrt{X_i}} + \beta_2 \sqrt{X_i} + \frac{u_i}{\sqrt{X_i}}$$

OK

20

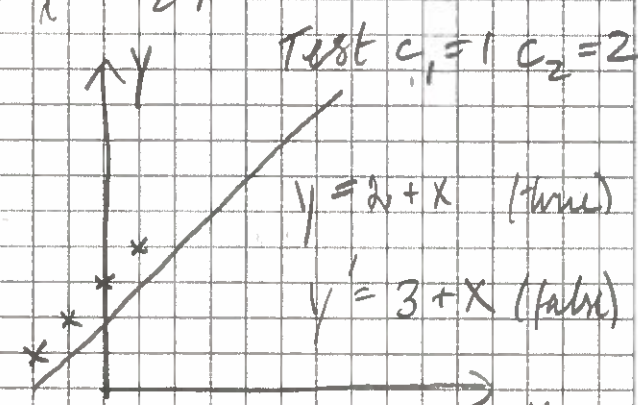
Uppgift 4

$$Y_i = \beta_1 + \beta_2 X_i + u_i \quad (\text{True})$$

$$(Y_i - c_1) = \beta_1 + \beta_2 (X_i - c_2) + u_i \quad (\text{False})$$

a)  $Y_i = \beta_1 + c_1 + \beta_2 (X_i - c_2)$

| $Y-1$ | $Y$ | $X$ | $X-2$ |
|-------|-----|-----|-------|
| 1     | 2   | 0   | -2    |
| 2     | 3   | 1   | -1    |
| 3     | 4   | 2   | 0     |
| 4     | 5   | 3   | 1     |



Guessing that  $\hat{\beta}_1$  will be biased but not  $\hat{\beta}_2$ .

$E(\hat{\beta}_i) = \beta_i$  unbiased

$$\hat{\beta}_2 = \frac{\sum (X_i - \bar{X})(Y_i - \bar{Y})}{\sum (X_i - \bar{X})^2} = \frac{\sum (X_i - c_2 - \bar{X} + c_2)(Y_i - c_1 - \bar{Y} + c_1)}{\sum (X_i - c_2 - \bar{X} + c_2)^2} = \hat{\beta}_2$$

$$\hat{\beta}_1 = \bar{Y} - \hat{\beta}_2 \bar{X} = \bar{Y} - c_1 - \hat{\beta}_2 (\bar{X} - c_2) \neq \beta_1$$

$\hat{\beta}_1$  is biased and  $\hat{\beta}_2$  is unbiased  
 Show that!

/10

Oppgaves

$$a) \quad Y = \beta_1 + \beta_2 X + u_i \quad X_i^* = \frac{X_i}{2}$$

$$\hat{\beta}_1^* = \hat{\beta}_1 \quad \hat{\beta}_2^* = 2 \hat{\beta}_2$$

False, only  $\hat{\beta}_2$  is changed OK

b) False  $Y_i$  is the dependent variable, a measurement error in  $X_i$  can introduce  $\text{Cov}(X_i, u_i) \neq 0$  OK

c) False. The DB test is used to detect autocorr. in disturbance terms OK

d) False, the coeff. of correlation is  $-1 < r < 1$  not the COV. OK

e) True. When  $V(u_i) = \sigma_i^2$  and the variance changes with i.e.  $X_i$  there is heteroscedasticity OK/3

f) True. The number of runs  $R \sim t$  under  $H_0$ :  $R$  is random when  $N_1 > 10$  and  $N_2 > 10$ . OK

1/6